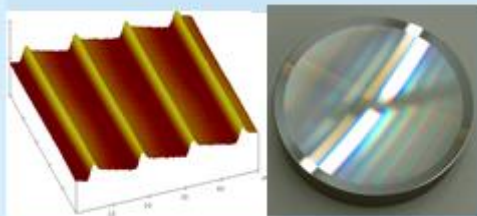
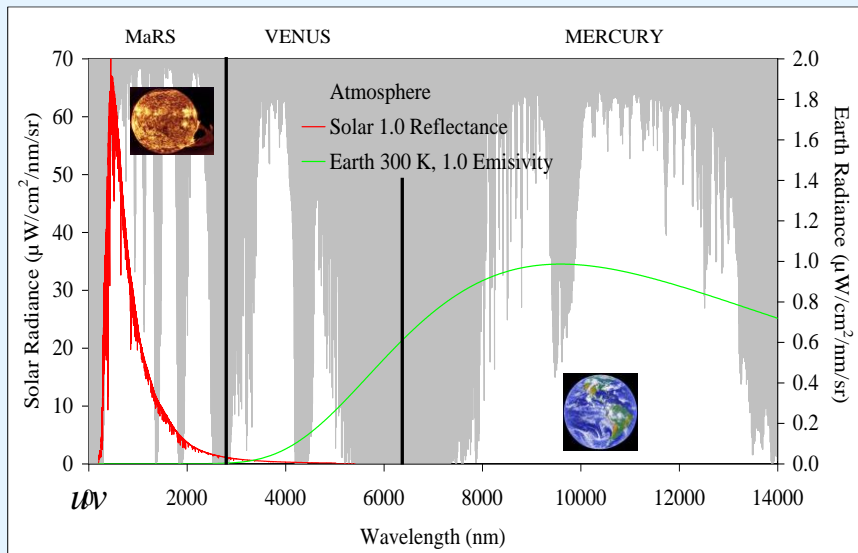


# Imaging Spectrometer Design for high data fidelity

## Design and Technology



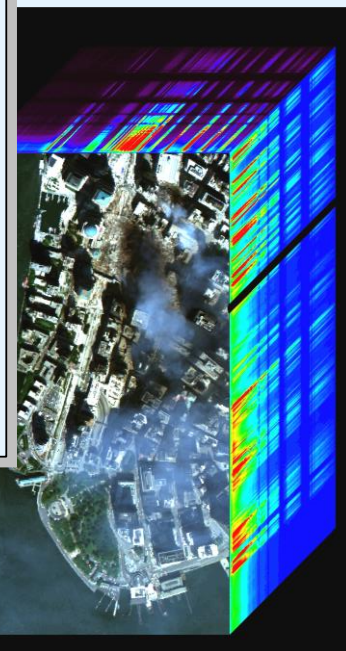
## Optical Spectrum



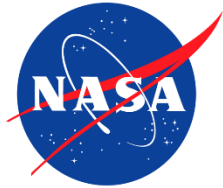
**Pantazis Mouroulis**

**Jet Propulsion Laboratory,  
California Institute of  
Technology**

## Results



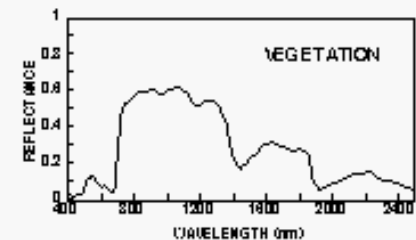
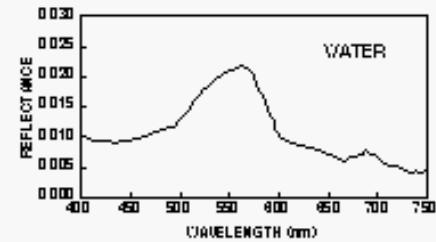
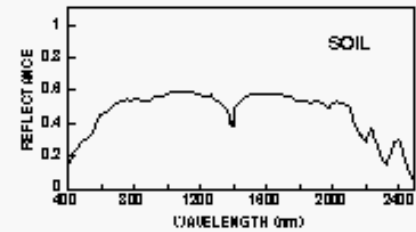
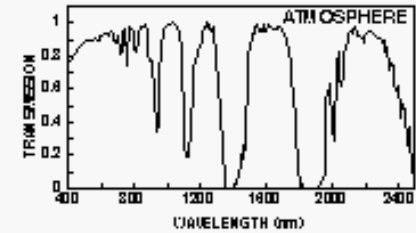
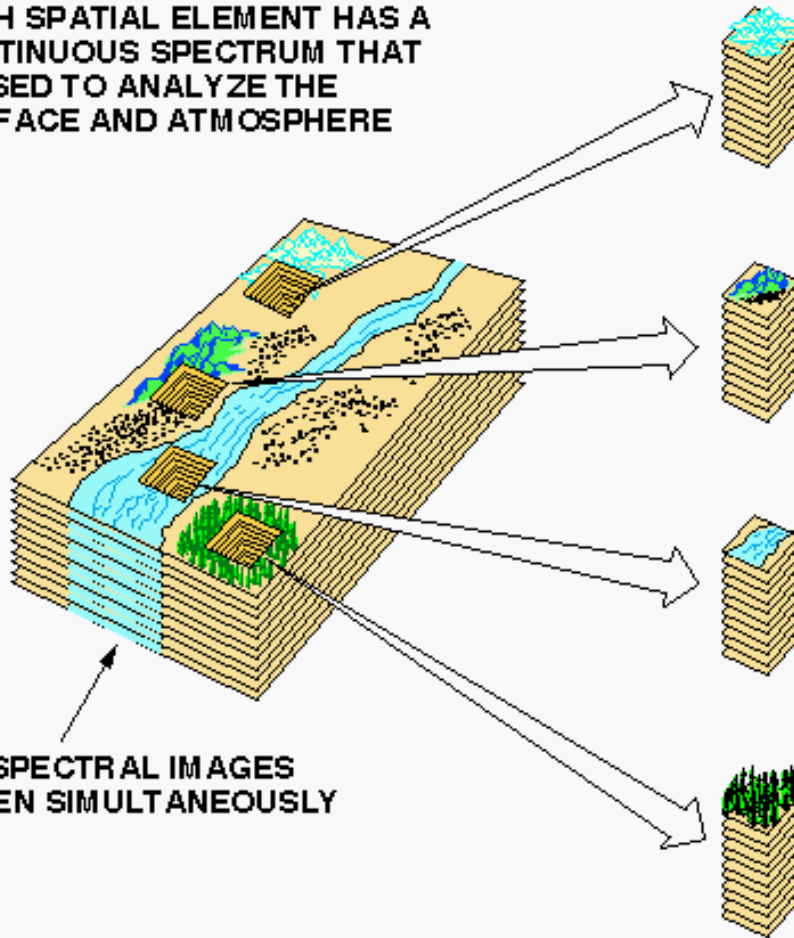
*AVIRIS Assessment of  
Asbestos, Fires, and Debris  
World Trade Center  
September 16, 2001*

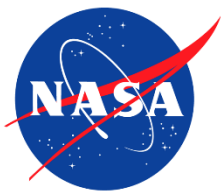


# Imaging Spectroscopy

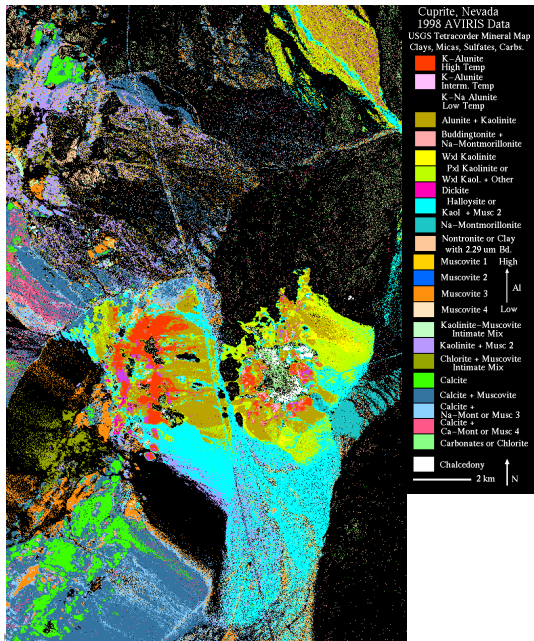
EACH SPATIAL ELEMENT HAS A CONTINUOUS SPECTRUM THAT IS USED TO ANALYZE THE SURFACE AND ATMOSPHERE

224 SPECTRAL IMAGES TAKEN SIMULTANEOUSLY

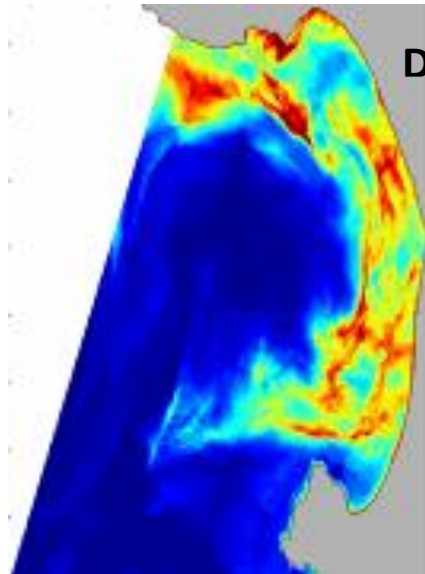




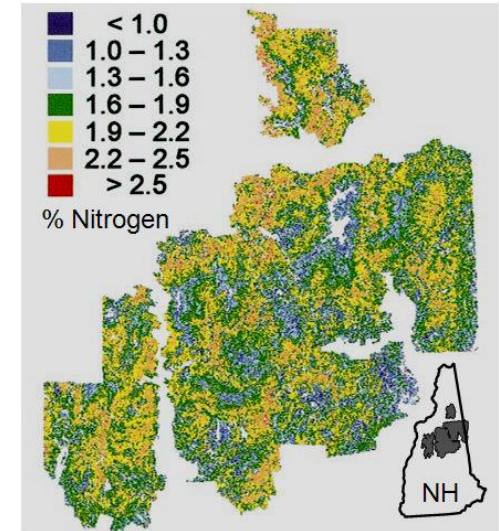
# Imaging spectroscopy reveals the composition and condition of the Earth's surface



Material identification



Hazards and episodic events



Vegetation health and productivity

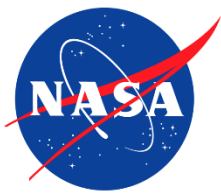
## **Imaging spectrometers in the solar system:**

VIMS (Saturn), Omega, CRISM (Mars), M3, HySI (Moon), VIRTIS

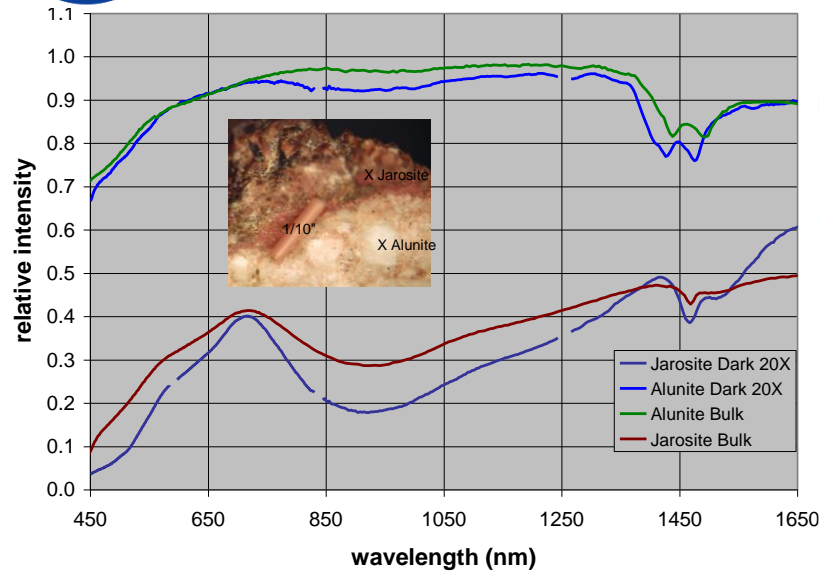
## **Imaging spectrometers orbiting Earth:**

Hyperion, MERIS, Artemis, HICO plus several airborne systems

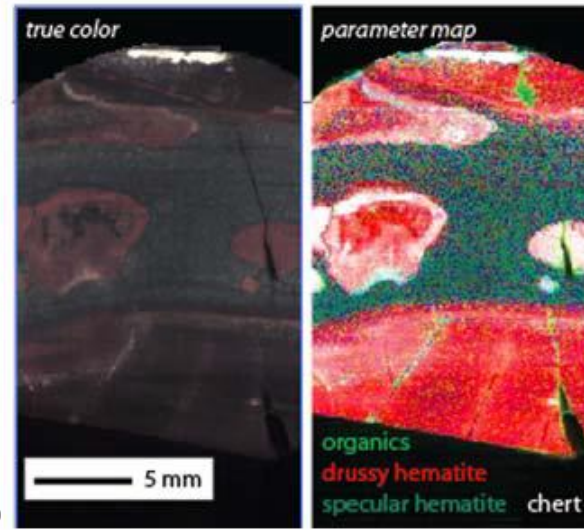




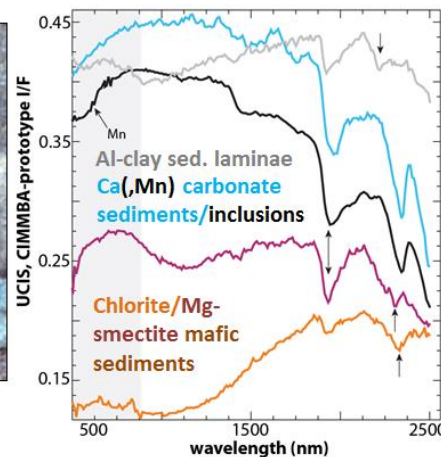
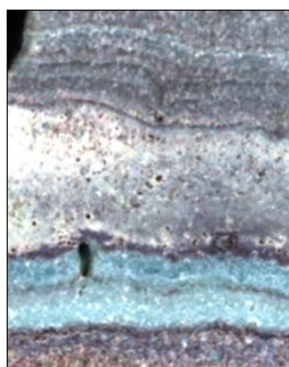
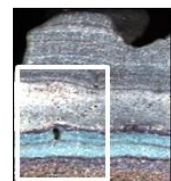
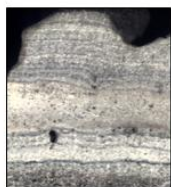
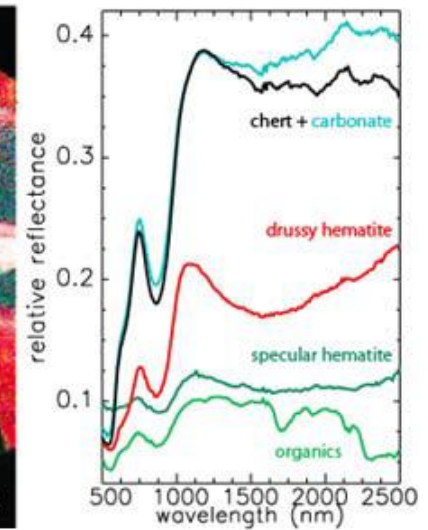
# REFLECTANCE MICROSPECTROSCOPY



Bulk and microscopic spectra comparison

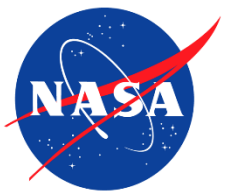


Banded iron formation: RGB/860,1750,2210 nm mapping of mineral phases. Single pixel or 3x3 spectra reveal Fe(III) oxides, chert & organics

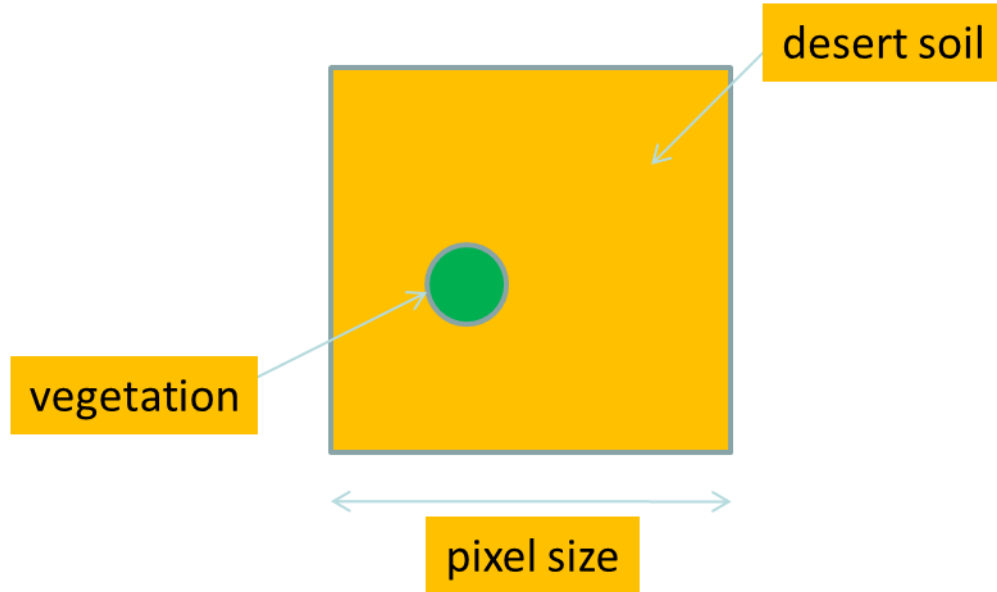


Stromatolite in visible and SWIR pseudocolor. Single grain resolution within the sandstone & single pixel spectra from location show distinctive sources of sediments and two generations of carbonate. Above the carbonate are aluminum-rich clay minerals and below it are clay minerals that include magnesium-rich chlorites and smectites.

Mouroulis, et al, *Appl. Spectrosc.* 62, 2008  
Van Gorp et al, *J. Appl. Rem. Sens.* 8, 2014



## Imaging spectroscopy vs. Hyperspectral imaging

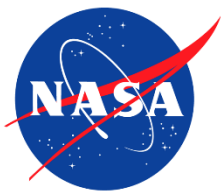


Vegetation is not resolved spatially (not imaged) but it can be resolved spectrally. Requirement for resolving spectral mixtures is very tight, ~1% or as small as possible.

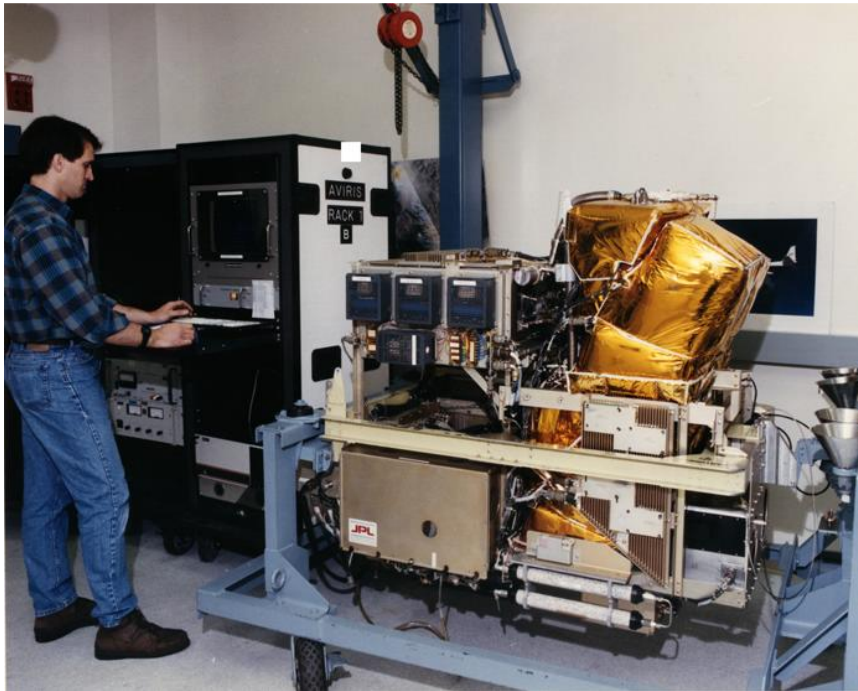
Imaging spectroscopy: Identification through spectroscopy of spatially resolved or unresolved features, together with a map of their location.

“Hyperspectral imaging” implies a spatially resolved image with too many spectral bands.

Not mere semantics: Spatial resolution requirements are different if imaging is paramount (critical vs.  $>$  Nyquist)



# Airborne Visible/Infrared Imaging Spectrometer

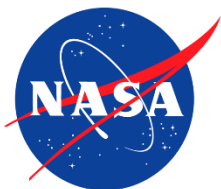


AVIRIS is designed with  $200\text{ }\mu\text{m}$  detectors and F/1 optics. It is hard to imagine larger detectors or faster optics.

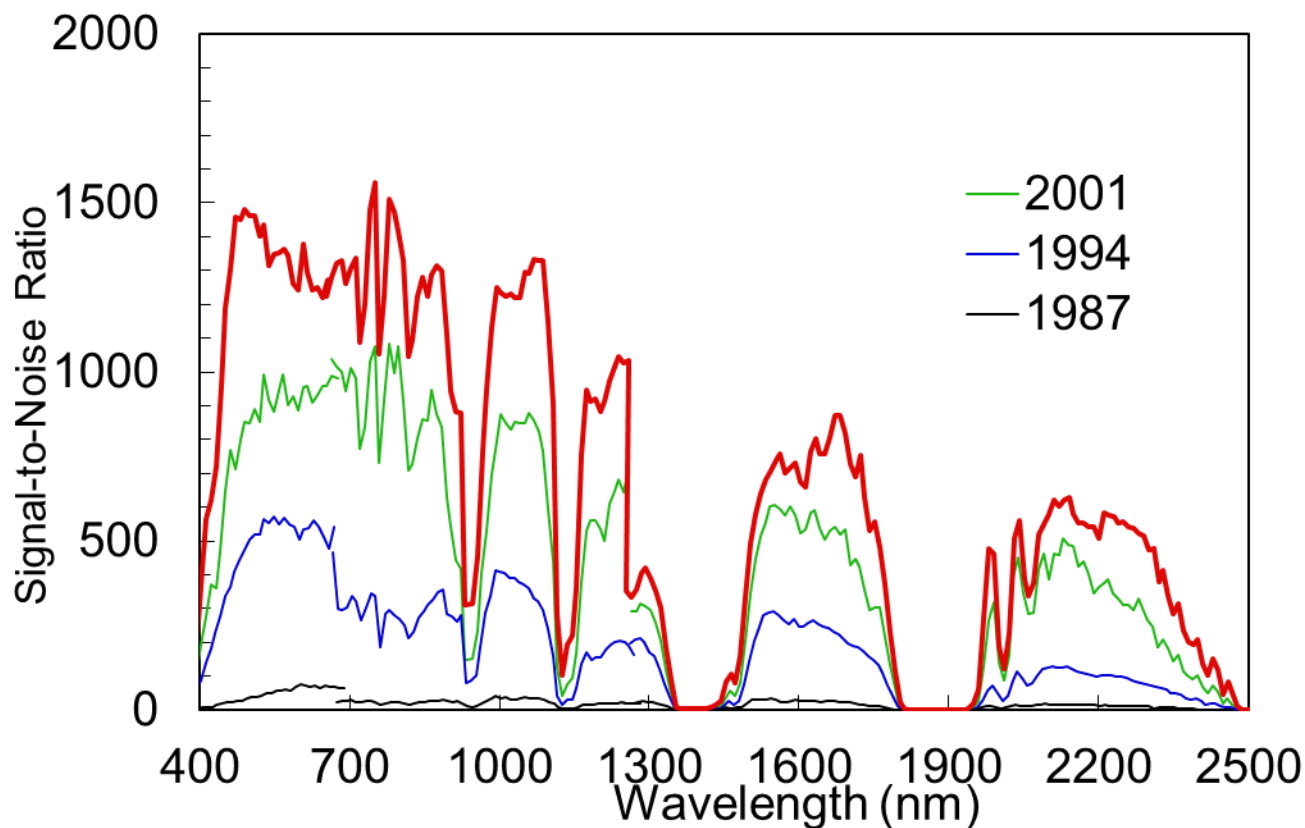
First flight 1987, has flown every year since 1989.

*Vane et al, Rem. Sens. Environment 44, 1993*

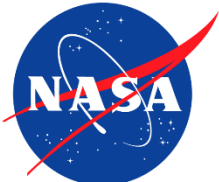
*Green et al, Rem. Sens. Environment 65, 1998*



## AVIRIS SNR through the years



Continuous improvements and upgrades have kept AVIRIS at the forefront of airborne science.



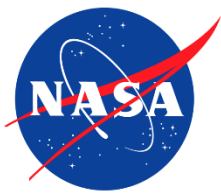
# Response Uniformity

- Any point on the ground yields calibrated, physically plausible spectral signature
- A spectral signature arises from a well-defined area on the ground

Maximum uniformity is achieved by a whiskbroom sensor with a single fiber connecting telescope and spectrometer.

AVIRIS is close to ideal (four distinct fibers connected to four spectrometers)





# COMPACT INSTRUMENTS ENABLED BY PUSHBROOM ARCHITECTURE

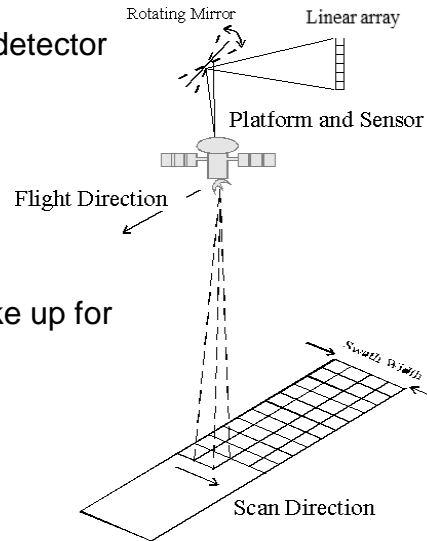
## WHISKBROOM

Inherently uniform  
(all spectra acquired by same detector array)

Easier to calibrate  
(linear detector array)

Inherently large  
(requires large aperture to make up for short integration time)

Requires scan mirror



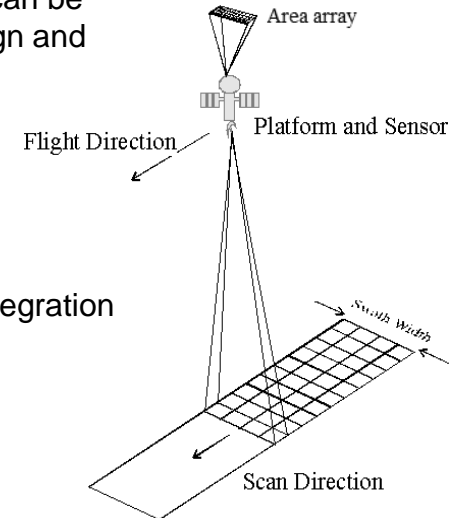
## PUSHBROOM

Inherently non-uniform – but can be made uniform by careful design and implementation

Harder to calibrate  
(area detector array)

Inherently small  
(takes advantage of longer integration time)

No moving parts

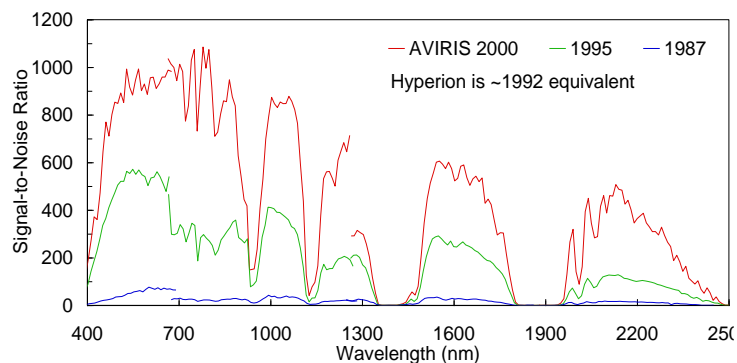


By integrating hundreds/thousands of simultaneous spectrometers on a single FPA, the pushbroom architecture achieves great size reduction, but requires also significant technology development and effort to achieve the same spectral purity, that is, eliminate spatial/spectral crosstalk.

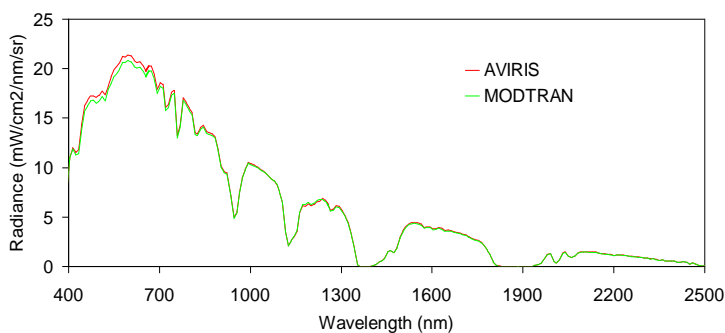


## *What is needed in the instrument/measurement:*

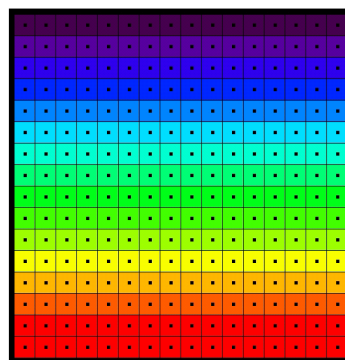
- High Signal-to-noise ratio required for molecular spectroscopy



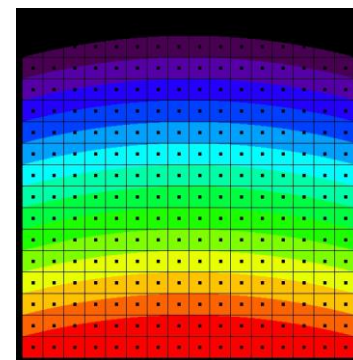
- Excellent calibration for quantitative results (spectral, radiometric, spatial)



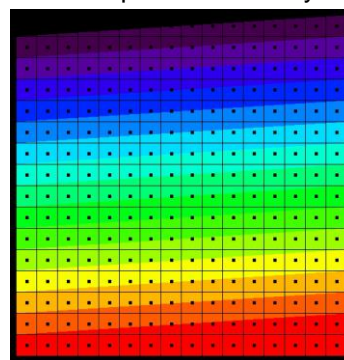
- Uniformity is required for spectroscopy in the image domain



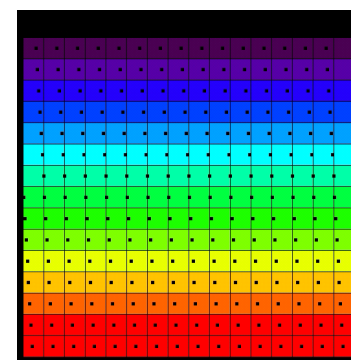
✓ Required Uniformity



✗ Failure by "frown"



✗ Failure by twist

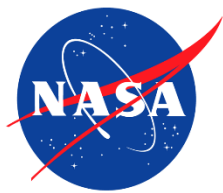


✗ Failure by  
Spectral-IFOV-shift 4-1

Geometric aspects of uniformity

*Green, Appl. Opt. 37, 1998*

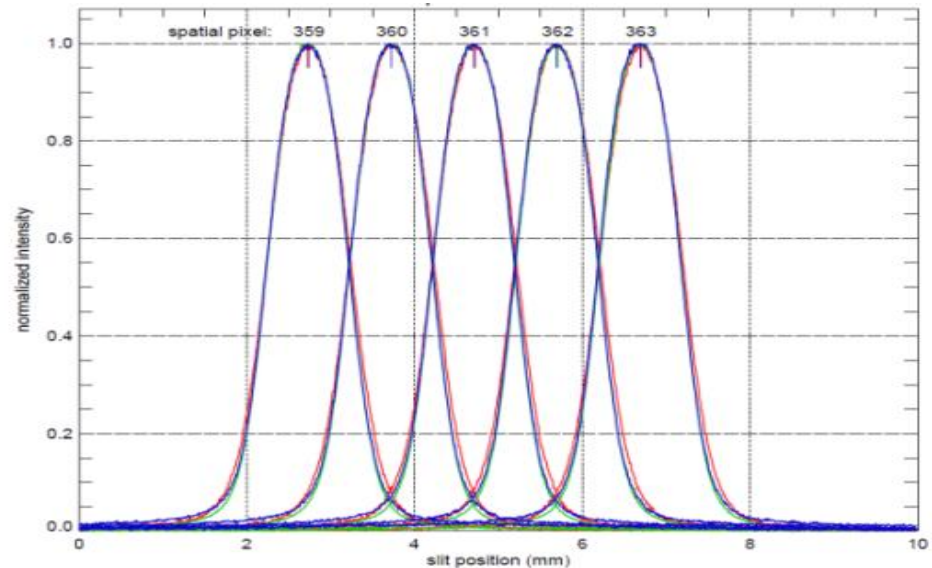
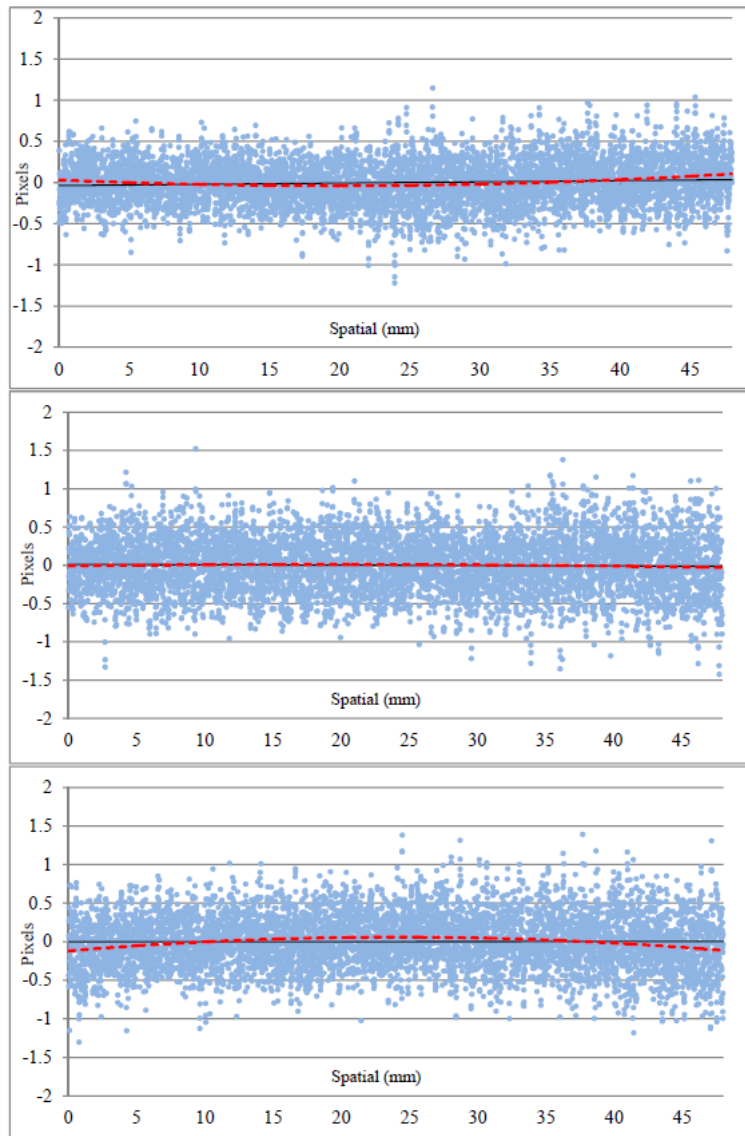
*Mouroulis & McKerns, Opt. Eng. 39, 2000*



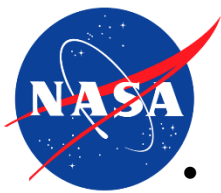
# How well can geometric aspects of uniformity be corrected?

- Demonstrated to date  $< 1\%$  smile ( $< 300$  nm) over 48 mm slit
- $< 2\%$  keystone ( $< 600$  nm) over 400-2500 nm band

*with proper tolerancing, alignment, and measurement techniques*



Bender et al, Proc. SPIE 9222 (2014)  
Bender et al, Proc. SPIE 8158 (2011)



## Non-geometric aspects of uniformity

- Spectral uniformity against spatial field: all “spectrometers” have the same calibration in terms of spectral response shape and width
- Spatial uniformity against wavelength: all colors arise from same patch on the ground

Even if detailed calibration is attempted, data extraction and correction algorithms become extremely complicated by having to account for different calibration for every pixel.

Variation of the response function shape and width causes similar effects as the variation in centroid location.

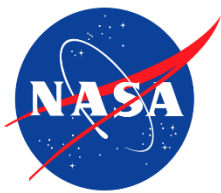
Full characterization accounts for any variation of light spilling outside the pixel.

If response functions are well approximated by Gaussians or similar forms, variation can be characterized in terms of first and second moments, or centroid and FWHM.

*Green, App. Opt. 37, 1998*

*Mouroulis, Green & Chrien, Appl. Opt. 39, 2000*

*Skauli, Opt. Express 20, 2012*



# Response function computation and assessment

Slit decouples telescope from spectrometer in one direction:

This means (to a first approximation):

- Along-track spatial response function (ARF) depends on front optic only
- Cross-track spatial response function (CRF) depends on the complete system (coherent coupling of front optics and spectrometer aberrations)
- Spectral response function (SRF) depends on the spectrometer only

First approximation means incoherent approximation that ignores slit diffraction.

Slit causes incident light to be diffracted outside the spectrometer aperture. This is ignored in raytrace models and in all raytrace-based wavefront models.

Partially coherent computation accounts for slit diffraction but is labor and resource intensive.

Incoherent approximation is generally good to  $< \sim 15\%$  in absolute terms, and significantly better in relative terms (e.g. determining difference between similar systems, different field points in the same system, etc.)

*Mielenz, J. Opt. Soc. Am. 57, 1967*

*Mouroulis & Green, Proc. SPIE 6667, 2007*





# Response Function Computation

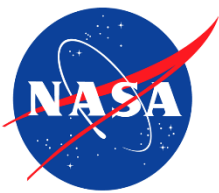
$$\text{ARF} = \text{rect}(y_0) \otimes \text{LSF}_T(y) \otimes \text{rect}(y_t)$$

$$\text{CRF} = \text{LSF}_{\text{sys}}(x) \otimes \text{DET}(x)$$

$$\text{SRF} = \text{rect}(y_0) \otimes \text{LSF}_{\text{sp}}(y) \otimes \text{DET}(y)$$

Incoherent approximation equivalent:

- In ARF computation, the spectrometer is ignored. Equivalent to placing a large detector immediately behind the slit (collects all light).
- In CRF computation, front optics and spectrometer aberrations are added as phase terms without considering the wavefront clipping by the slit.
- In SRF computation, the front optic is ignored. Equivalent to illuminating the slit with an integrating sphere (no aperture present before the slit).



# Telescope design principles

1. Zero transverse chromatic aberration (or  $<1\%$  of a pixel)
2. Minimum (ideally zero) variation of response with wavelength – over 2.5 octaves
3. Maximum transmission over broad band
4. Close pupil matching with spectrometer not required (but oversize apertures)

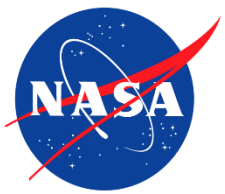
These imply:

1. Typically reflective telescope
2. Diffraction spread contained within the pixel/slit width (low F-number)
3. Minimum number of optical elements
4. Designs with virtual aperture stop permitted

Telescope designs available

- Three-mirror anastigmat (more mirrors possible, but accept transmission loss)
- Two-mirror modified Schwarzschild
- Cassegrain with field corrector if required (refractive or reflective corrector possible)

Purely refractive designs severely limited (some examples in Mouroulis Proc. SPIE 6667 (2007) and Fisher & Welch, Proc. SPIE 6062 (2006))



# Telescope design examples

TMA combines relatively compact size with the ability for wide field and relatively low F-number

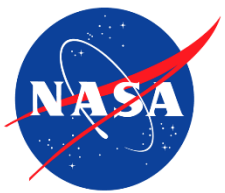
Preferred design for medium focal length and field. Unobscured.

Two-mirror telescope combines very low f-number with wide field but is large relative to focal length

Preferred choice for medium to short focal length, wide field, low f-number. Unobscured.

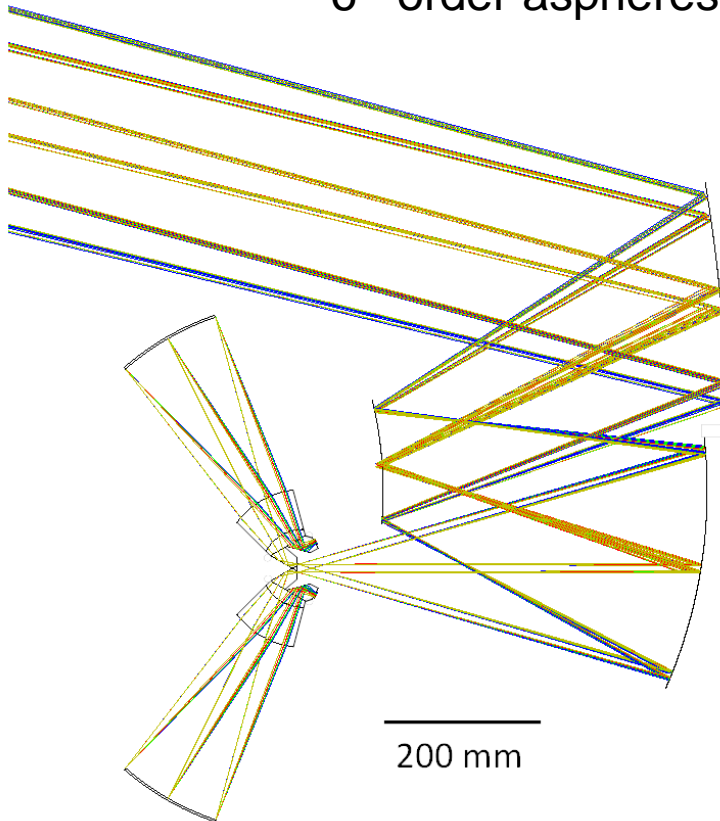
Cassegrain is needed for long focal length designs due to compact size.

Refractive or reflective corrective relays can widen field. Obscured.

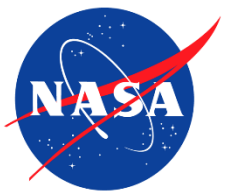


TMA example, 420 mm, F/1.8, 16 deg FOV, 18 um pixel size, 6400 cross-track pixels

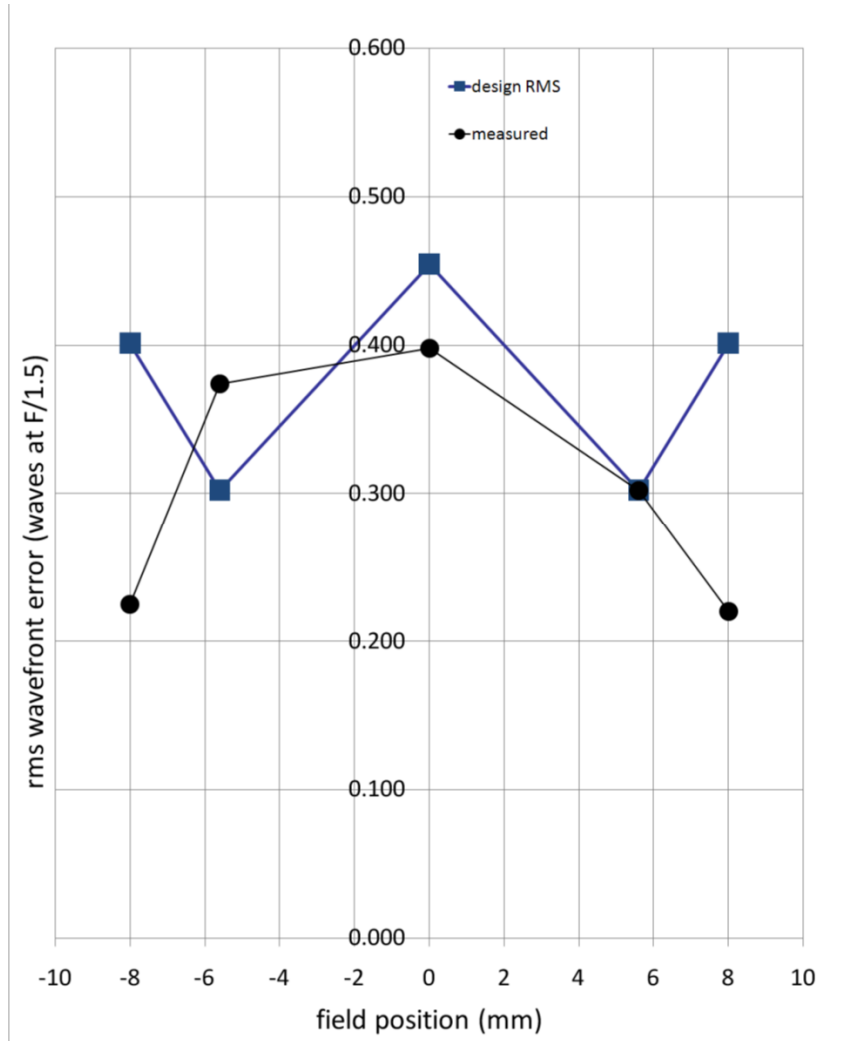
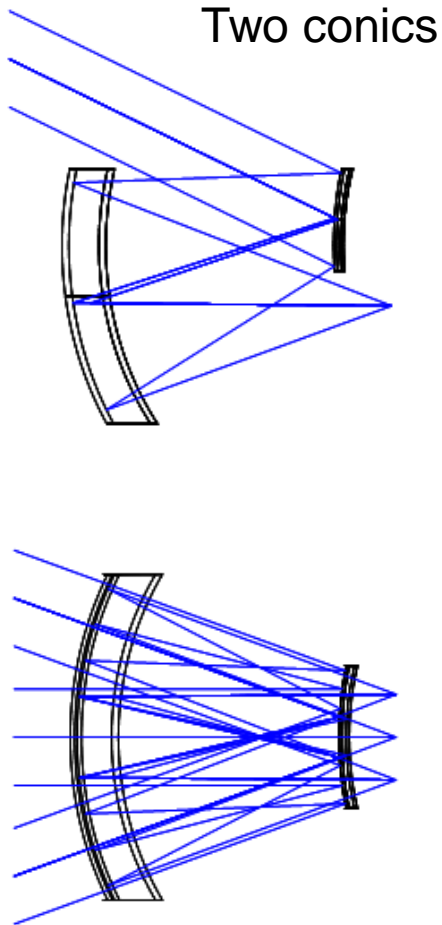
6<sup>th</sup> order aspheres



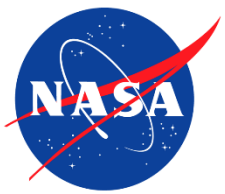
x-field	ensquared energy fraction	ensquared energy/diff. limit
1	0.87	0.96
-4	0.88	0.97
-6	0.86	0.95
-7	0.83	0.92
1	0.84	0.93
6	0.87	0.96
8	0.87	0.96
9	0.84	0.93



# TMA example, 30 mm, F/1.4, 33 deg FOV, 30 um pixel size, 640 cross-track pixels

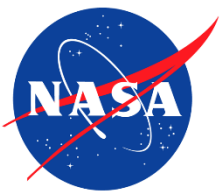






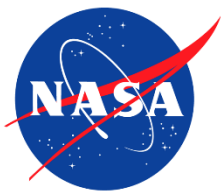
## Cassegrain:

- Field can be extended to over 1 degree with various types of correctors
- Achromatized refractive corrector with all  $\text{SiO}_2$  or  $\text{CaF}_2$  elements possible
- Reflective corrector with a 3-mirror relay is preferred due to both transmission and stray light control

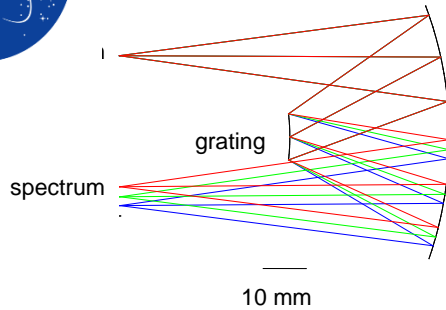


# Spectrometer design principles

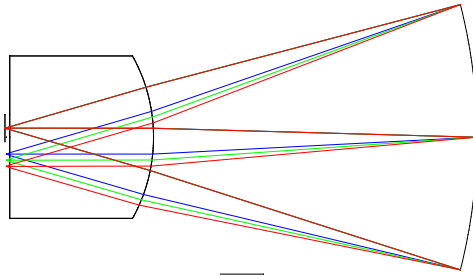
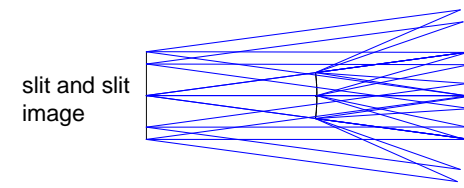
1. Geometric distortions controlled to 1% of a pixel at design (~3% after tolerancing)
2. Preferred stop location is at the grating or dispersive element
3. Accept degraded spot sizes to improve uniformity
4. Include uniformity operands in merit function
5. Maintain >75% of diffraction energy within pixel at all wavelengths and fields
6. Integrate (deterministic part of) stray light assessment into first design
7. Assess uniformity and image quality in terms of spatial and spectral response functions, and not wavefront, MTF, rms spot size, etc. etc., except as any of the faster-to-compute measures can be shown to correlate with response functions



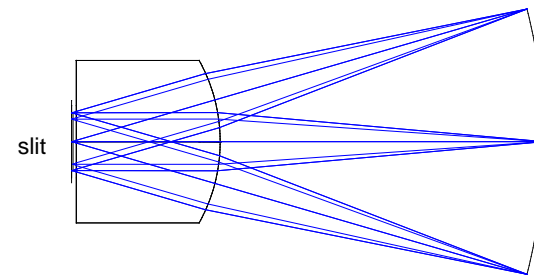
# Concentric spectrometer forms are ideally suited to pushbroom architectures



Offner

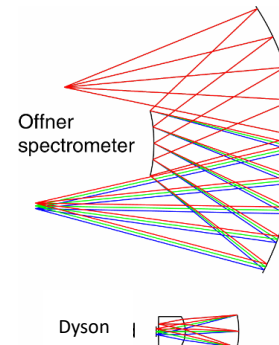


Dyson

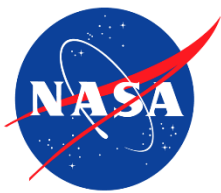


Offner	Dyson
All reflective (broad band, athermalization)	High throughput
Can reach high spectral resolution	Miniature size
Weaker detector ghosts	Easiest alignment

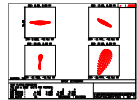
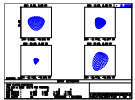
Size comparison between Offner and Dyson with the same specifications (@F/1.6)



Dyson, J. Opt. Soc. Am.(1959), Offner, Opt. Eng. (1975), Mertz, Appl. Opt. (1977), Kwo et al, Proc. SPIE 818 (1987), Maker et al, Proc. SPIE CR62 (1996), Mouroulis, Proc. SPIE 7298 (2009)

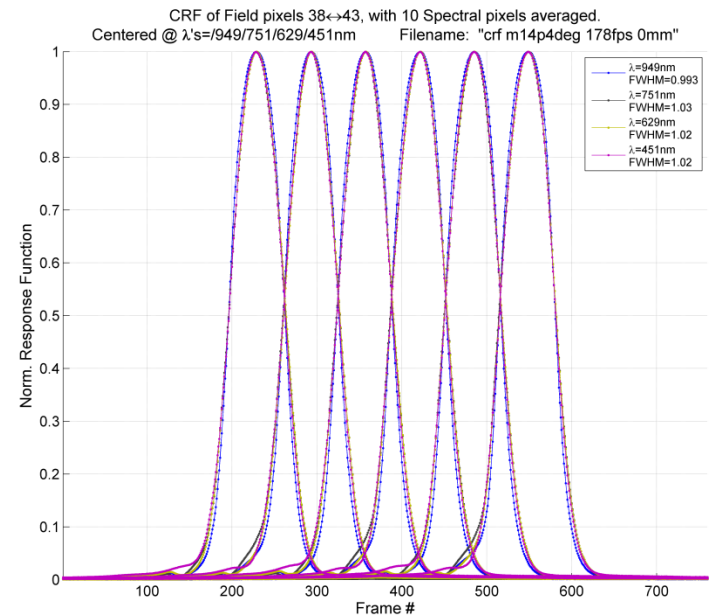
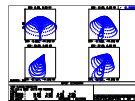


These design and assembly/alignment techniques lead to high uniformity



High uniformity through wavelength of cross-track spatial response example

Aberration may be intentionally increased to improve uniformity



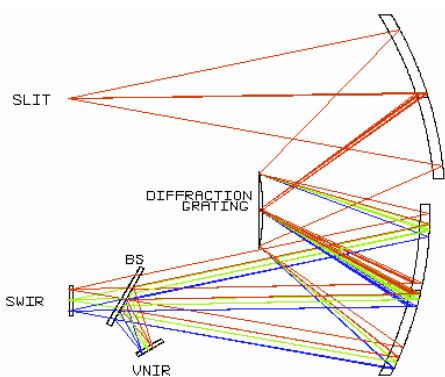
# Spectrometer design examples





## Offner imaging spectrometer system development at JPL

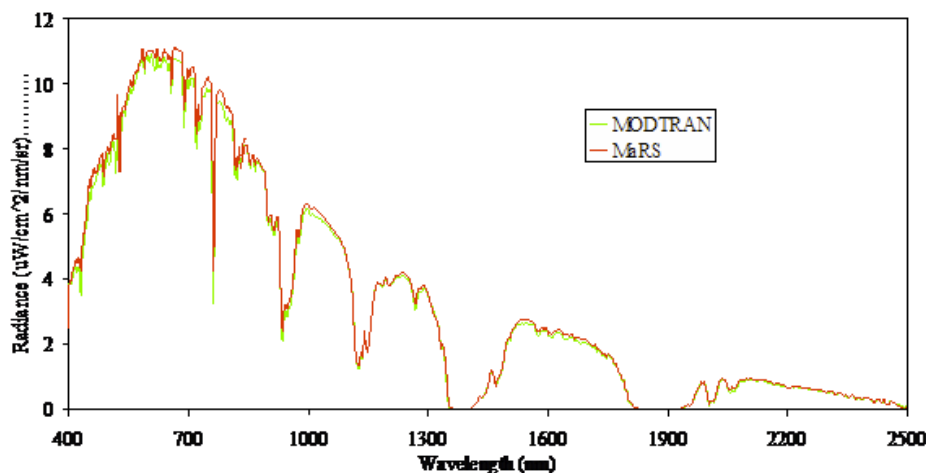
- 2006: MaRS (airborne)
- 2008: M3 (Moon orbit)
- 2011: Next Generation Imaging Spectrometer (airborne)  
CAO, NEON, AVIRISng
- 2012: MSS (airborne)
- 2012: Ultra-compact Imaging Spectrometer (in-situ or orbit)



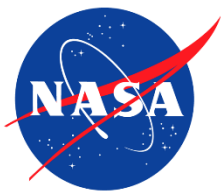
MaRS 2-FPA design



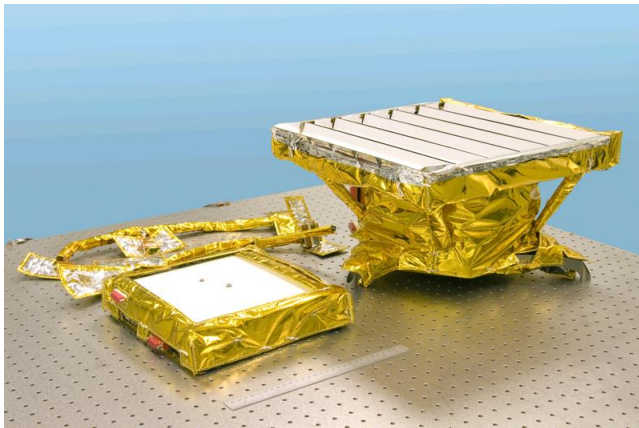
Installation



Radiometric calibration >97%



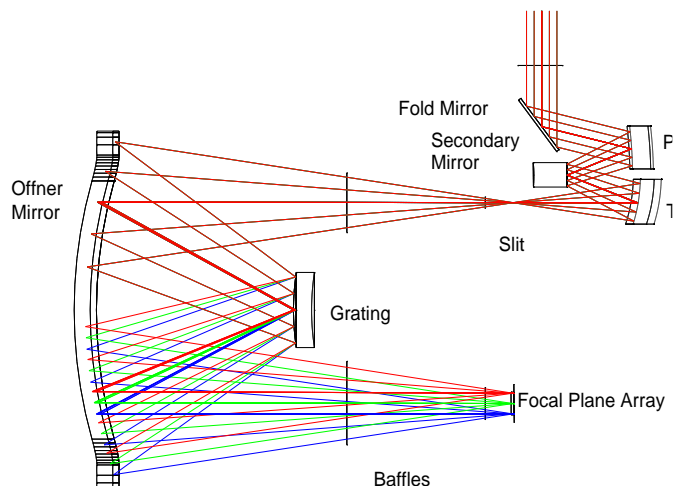
# The Moon Mineralogy Mapper (M3) on Chandrayaan I



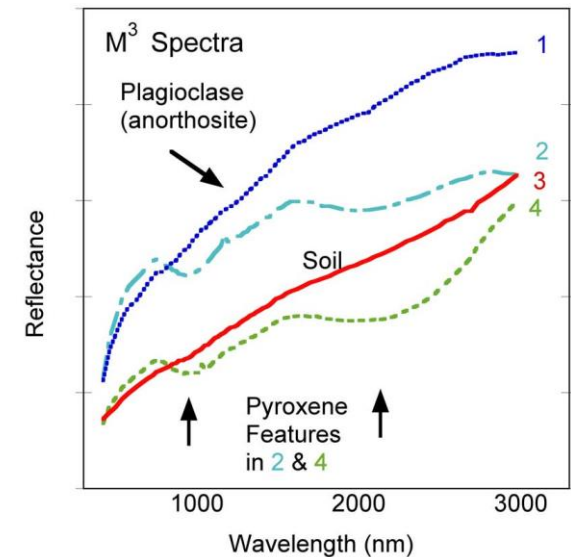
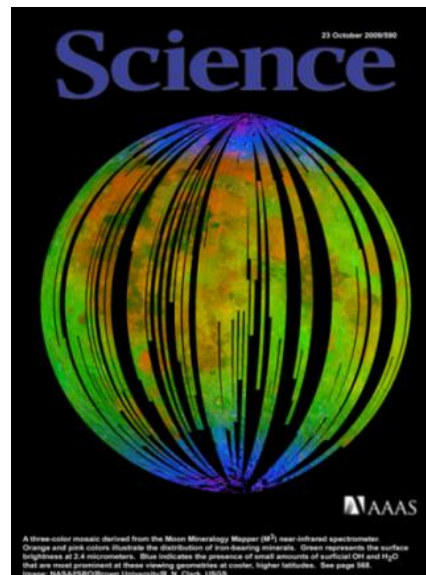
Launched 22 Oct. 2008

8 kg mass, 24 month build

- 430-3000 nm band
- 10 nm sampling
- 600 cross track pixels



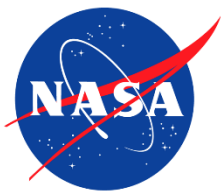
1-FPA, 4-mirror telescope



Pieters et al, Science 326, 2009

Green et al, J. Geophys. Res. Planets 116, 2011

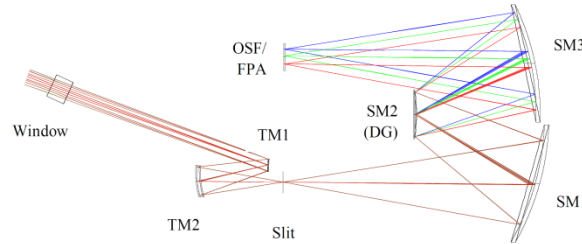
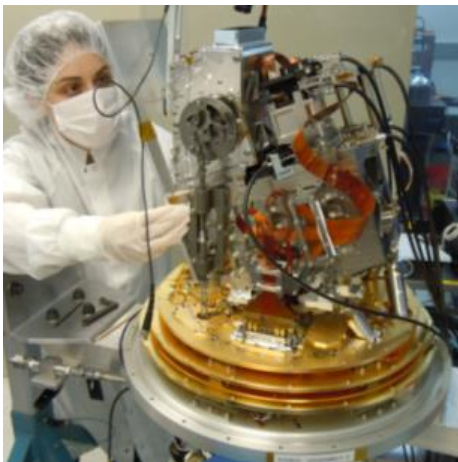
Mouroulis et al, Opt. Engineering 46, 2007



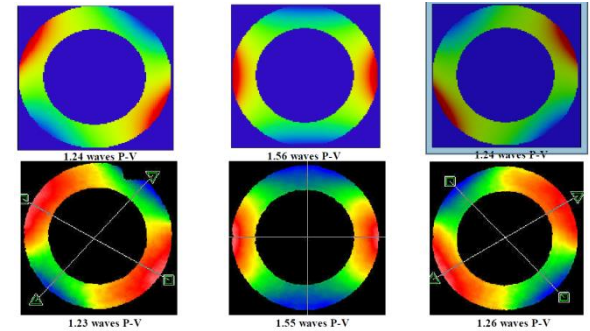
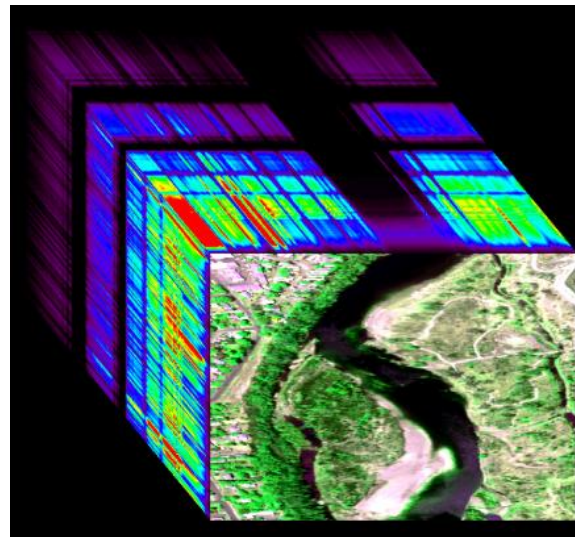
# Next Generation Airborne Imaging Spectrometer



NGIS deployment

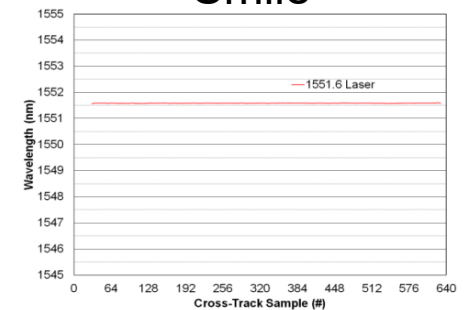


1-FPA, two-mirror telescope

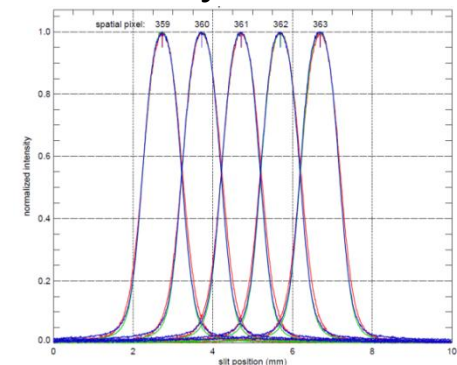


Alignment techniques to achieve high uniformity

“Smile”



“Keystone”

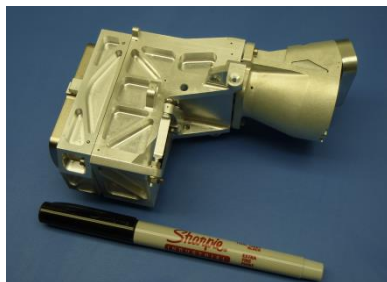


*Bender et al, Proc. SPIE 7812, 2010*  
*Bender et al, Proc. SPIE 8158, 2011*

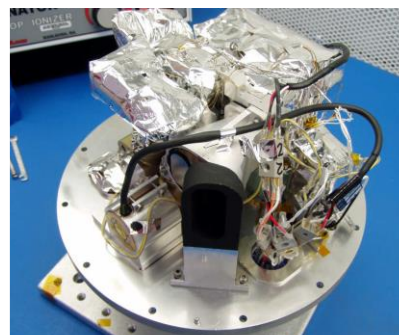




# Offner imaging spectrometer system development at JPL Ultra-compact Imaging Spectrometer (UCIS) for in-situ mineralogy



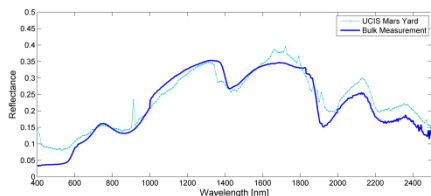
Miniaturized full-range (500-2600 nm) spectrometer system



Optical bench



Full system in vacuum enclosure



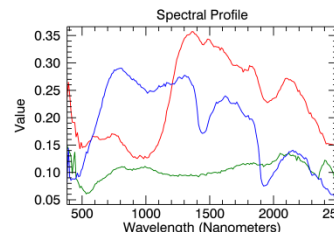
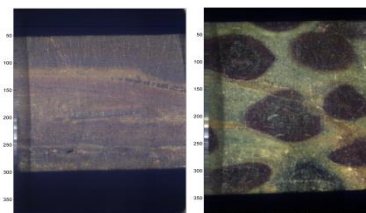
Critical spectral bands identified



Wide angle scan with a spectrum recorded for every point

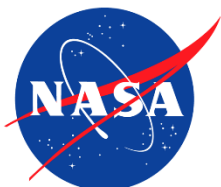


In the field



Microscopic mode:  
spatial resolution  
80  $\mu\text{m}$

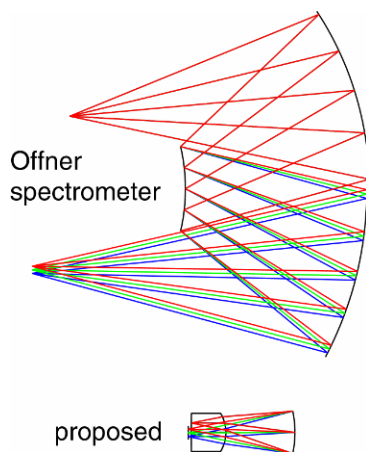
Van Gorp et al, Proc. SPIE 8158, 2011  
Van Gorp et al, J. Appl. Rem. Sens. 8, 2014



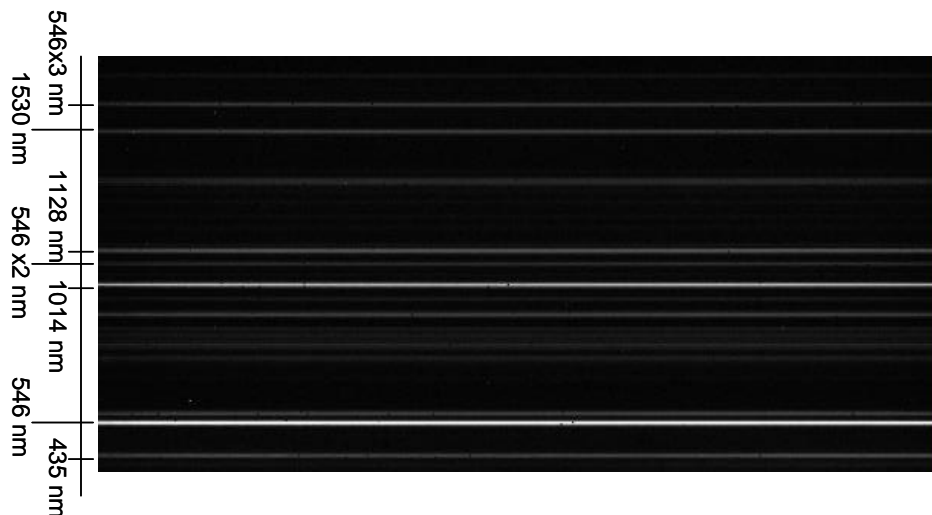
## Dyson imaging spectrometer development at JPL

Dyson design offers even more compact size, higher throughput, and low polarization sensitivity.

Size comparison between Offner and Dyson with the same specifications (@F/1.6)



Test spectra from Hg lamp

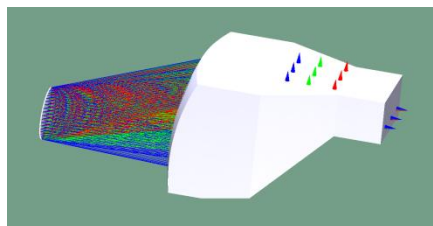


Complete assembly of Dyson spectrometer optics (400-1700 nm, F/1.8, 640 spatial elements)



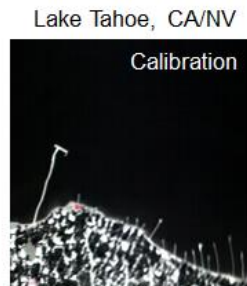
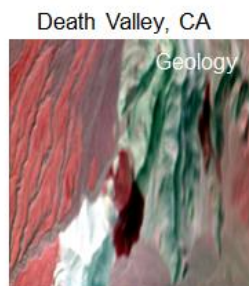
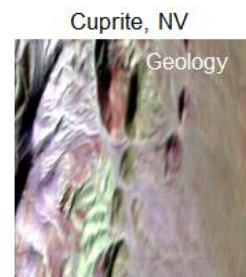


# HyTES: Hyperspectral Thermal Emission Spectrometer

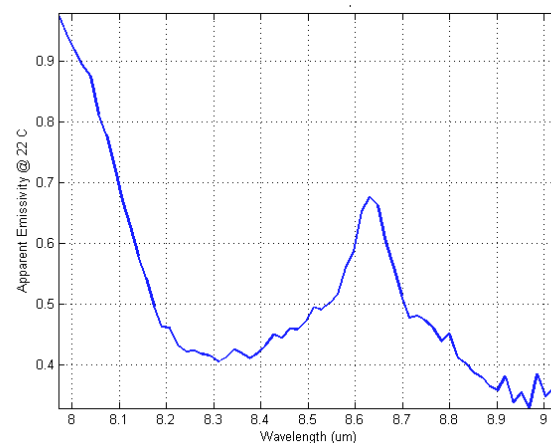


- 7.5-12  $\mu\text{m}$
- 50° FOV
- 512 spatial elements
- 256 spectral channels
- F/1.6 aperture

Miniature optical design

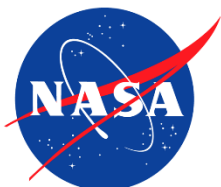


Bands 150 (10.08  $\mu\text{m}$ ), 100 (9.17  $\mu\text{m}$ ), 58 (8.41  $\mu\text{m}$ ), displayed at RGB each image is 495 x 512 pixels

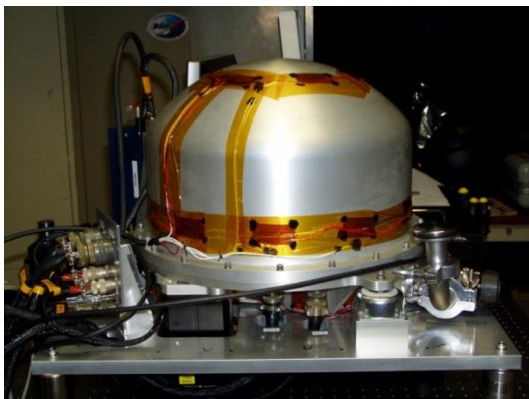


Measured emission spectrum of quartz

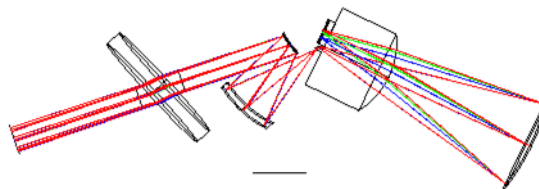
*Johnson et al, Proc. SPIE 7457, 2009*  
*Hulley et al, Atmos. Meas. Tech., 9, 2016*



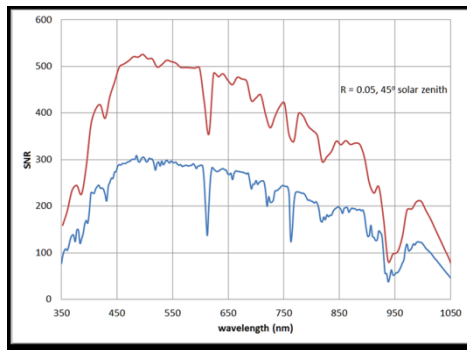
# Portable Remote Imaging Spectrometer (PRISM) Coastal Ocean Sensor



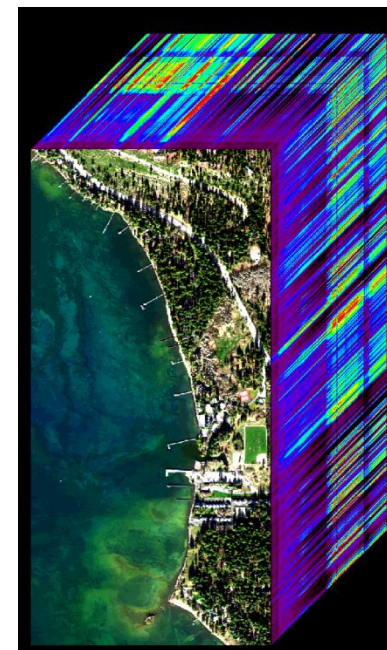
Sensor head installed in Twin Otter below



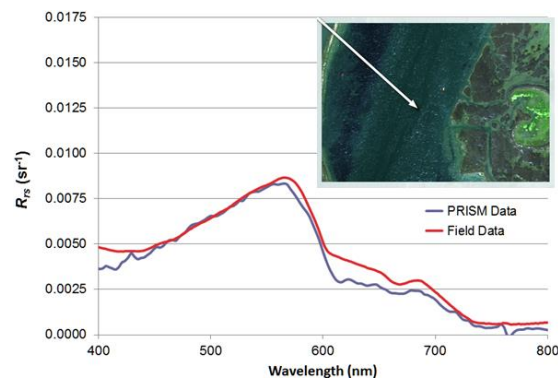
Fast and compact optical design that supports high uniformity and low polarization sensitivity



High Signal to Noise for dark targets



Spectral image cube from Lake Tahoe

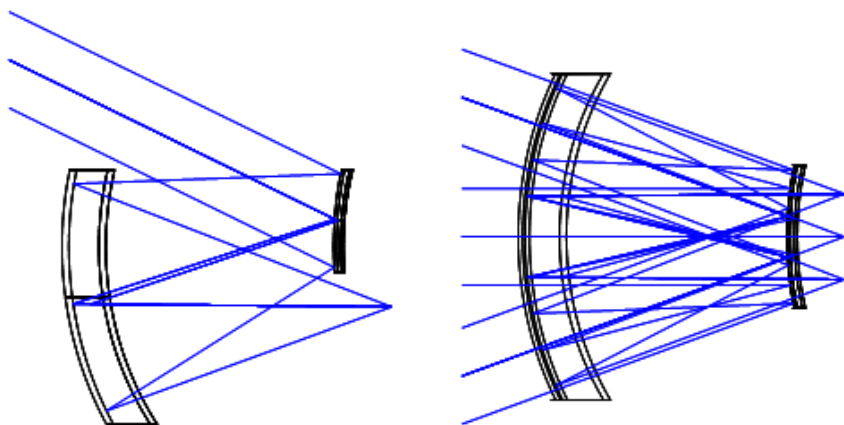


Excellent agreement between PRISM and in-situ measured spectra

Mouroulis, Green & Wilson, *Opt. Express* 16, 2008  
Mouroulis et al, *Appl. Opt.* 53, 2014

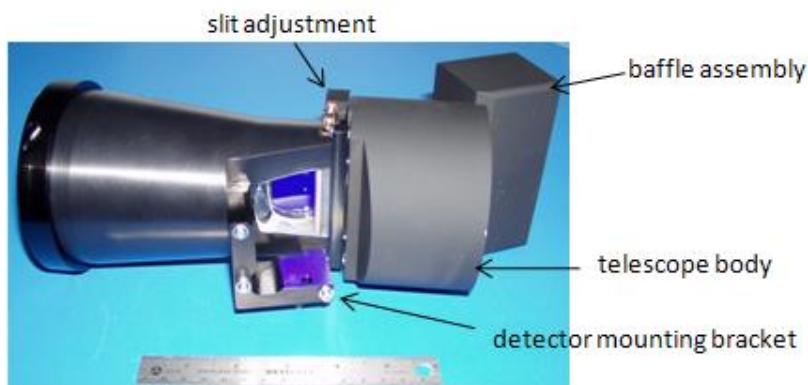
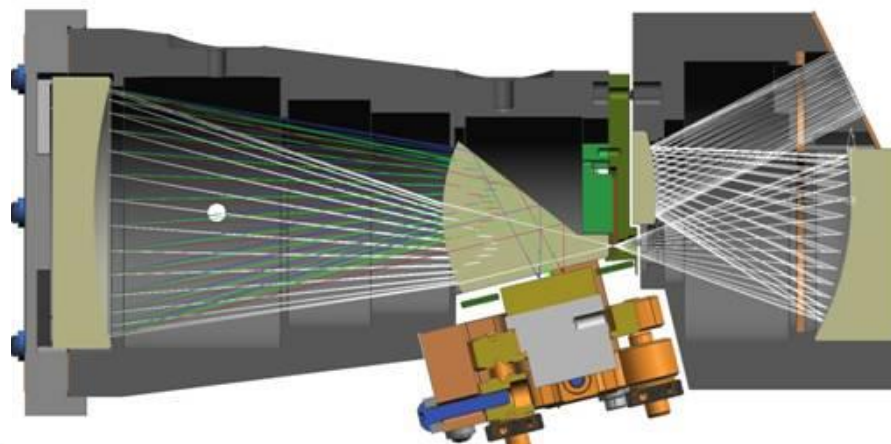


## Maximum throughput, wide field spectrometer



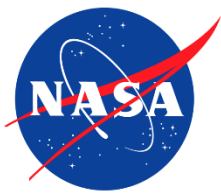
- Two axially centered conics
- Tolerant to misalignment

Two-mirror design, F/1.4, 33° FOV



*Mouroulis et al, Proc. SPIE 8032, 2011*

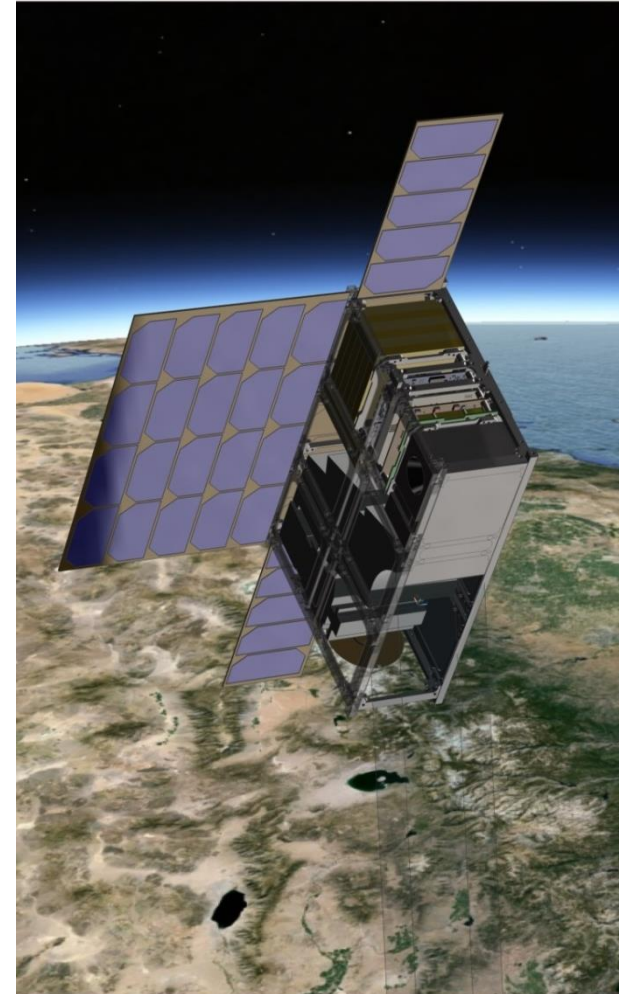




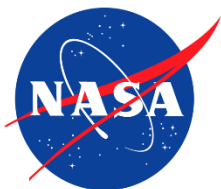
# Snow and Water Imaging Spectrometer (SWIS)

- A CubeSat-compatible imaging spectrometer (6U)
- High SNR
- High dynamic range
- On-board calibration
- More frequent/regular sampling relative to airborne instruments
- Intermediate to high resolution relative to global or flagship missions
- Relatively low-cost alternative

Addresses coastal waters and snow/ice cover applications

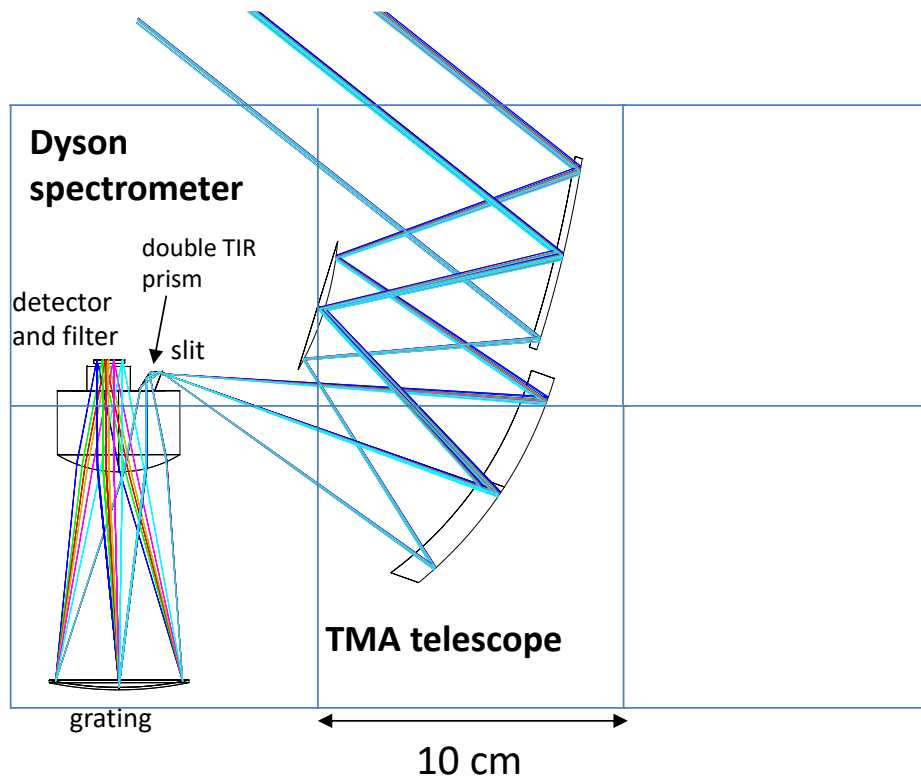


SWIS CubeSat, artist's concept



# SWIS instrument specifications

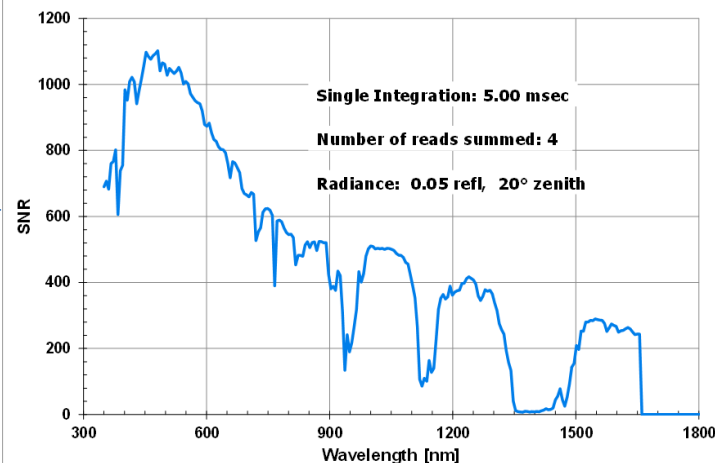
Spectrometer and telescope inside 6U CubeSat frame



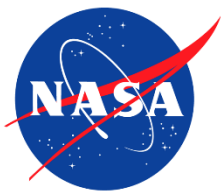
## SWIS specifications

Spectral range	350-1700 nm, single FPA
Spectral sampling	5.7 nm
Cross-track spatial elements	600 (+40 monitor)
Cross-track FOV	10°
Resolution	0.3 mrad
Detector pixel size	30 $\mu\text{m}$
Focal length	100 mm
F-no	1.8
Uniformity	95%

Signal to Noise Ratio: Summation to One Spatial Pixel

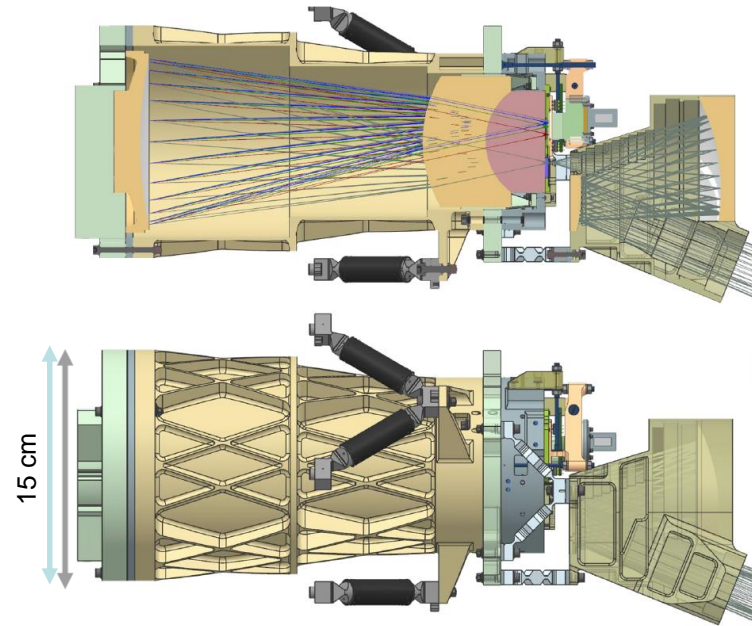


*Mouroulis et al, Proc. SPIE 9222, (2014)*



# The Compact Wide and the Advanced Land Imaging Spectrometer (CWIS and ALIS)

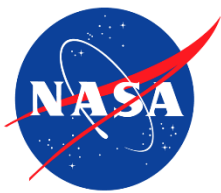
- Landsat swath and resolution challenging even for multispectral instruments (~6300 pixels cross track)
- Thematic Mapper (whiskbroom) finally abandoned in Landsat 8
- OLI replaces Thematic Mapper, pushbroom plus discrete filters
- Imaging spectrometer solution offers simultaneity of spectral bands and enhanced science capabilities
- Increase in number of spectral bands by an order of magnitude
- Challenging design, must be high SNR



*Van Gorp et al, Proc. SPIE 9222, 2014*

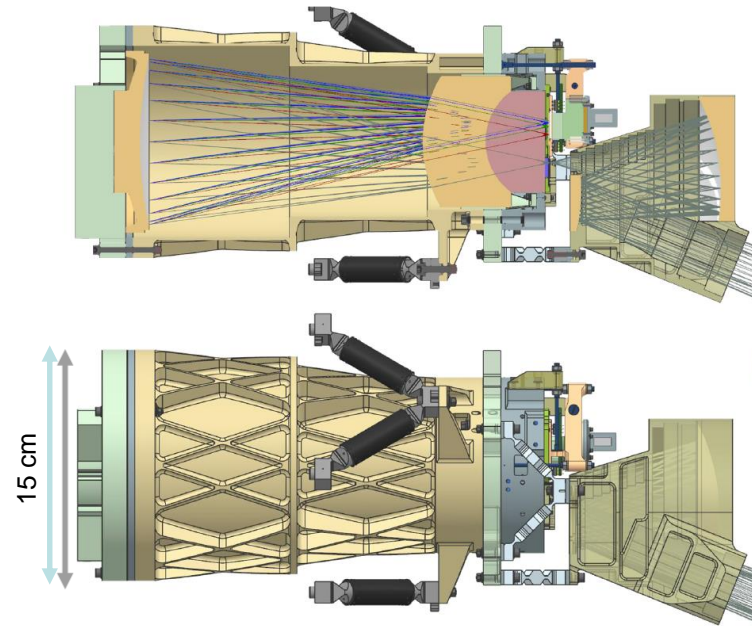
CWIS: 1600 x 30  $\mu\text{m}$  pixels

ALIS: 3200 x 18  $\mu\text{m}$  pixels



# The Compact Wide and the Advanced Land Imaging Spectrometer (CWIS and ALIS)

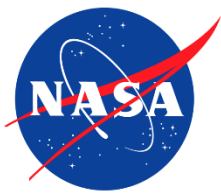
- Landsat swath and resolution challenging even for multispectral instruments (~6300 pixels cross track)
- Thematic Mapper (whiskbroom) finally abandoned in Landsat 8
- OLI replaces Thematic Mapper, pushbroom plus discrete filters
- Imaging spectrometer solution offers simultaneity of spectral bands and enhanced science capabilities
- Increase in number of spectral bands by an order of magnitude
- Challenging design, must be high SNR



*Van Gorp et al, Proc. SPIE 9222, 2014*

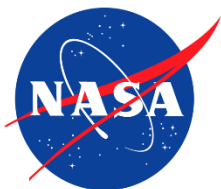
CWIS: 1600 x 30  $\mu\text{m}$  pixels  
ALIS: 3200 x 18  $\mu\text{m}$  pixels





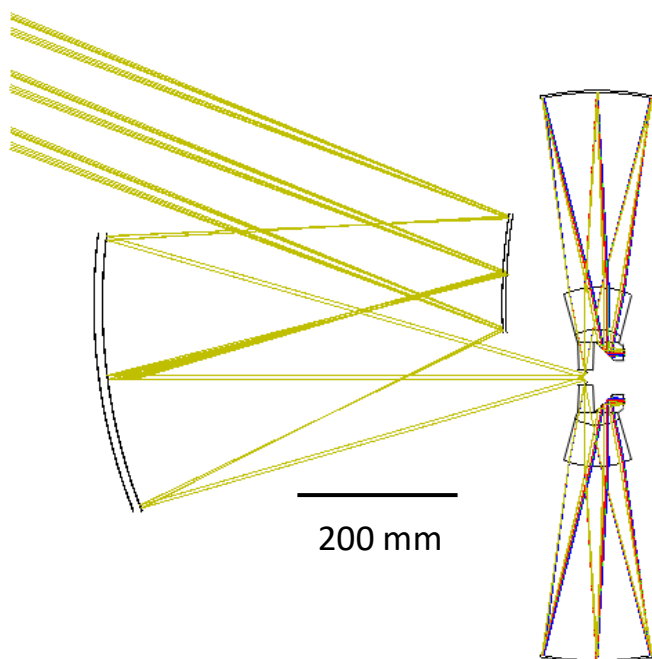
# ALIS SPECIFICATIONS

Parameter	Value
Scan type	Pushbroom
Cross-track spatial elements	6400 (2 x 3200)
Telescope focal length	420 mm
F-number	1.8
Telescope FOV	16° x 1.3°
Spectrometer magnification	-1
Detector pixel size	18 $\mu\text{m}$ square
Slit length (one spectrometer)	57.6 mm
Spectral range	380 – 2510 nm
Spectral sampling	6.8 nm per 18 $\mu\text{m}$ pixel
SNR	See Fig. 5
Spectral uniformity	90%
Spectral IFOV uniformity	90%



# ALIS Design and optical performance

Enclosed energy in 18  $\mu\text{m}$  width



Two-mirror telescope allows simple folding.  
TMA telescope also designed.

Wavelength	x-direction (spatial)	Fraction of diffraction-limited
380	0.94	0.95
630	0.89	0.90
1200	0.85	0.88
2500	0.88	0.94

Wavelength	y-direction (spectral)	Fraction of diffraction-limited
380	0.96	0.97
630	0.93	0.94
1200	0.92	0.94
2500	0.89	0.95

spectrometer

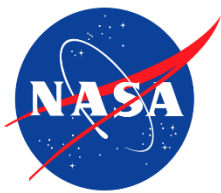


# ALIS Response Function Assessment

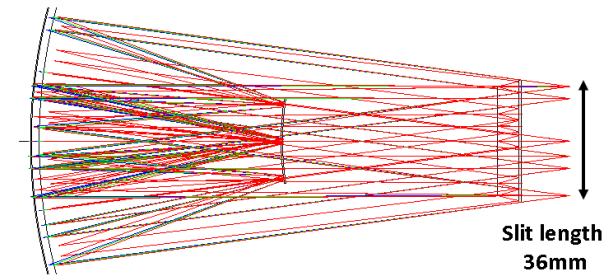
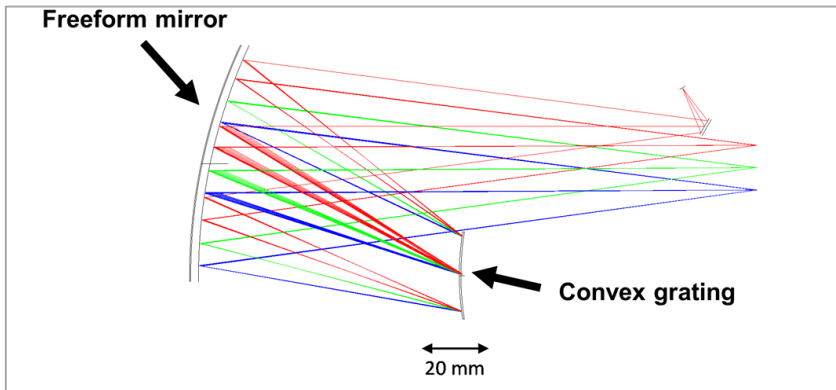
Distance from center of slit (mm)	SRF FWHM @380 nm (pixel fraction)	SRF FWHM @800 nm (pixel fraction)	SRF FWHM @1600 nm (pixel fraction)	SRF FWHM @2500 nm (pixel fraction)
0	1.31	1.33	1.35	1.42
11.25	1.32	1.35	1.36	1.4
18	1.33	1.38	1.37	1.39
22.5	1.33	1.39	1.38	1.39
28.8	1.33	1.39	1.37	1.44

wavelength	CRF FWHM at 1°	CRF FWHM at -4°	CRF FWHM at -6°	CRF FWHM at -7°
380 nm	1.12	1.1	1.13	1.26
800 nm	1.14	1.13	1.12	1.18
1600 nm	1.12	1.11	1.13	1.22
wavelength	ARF FWHM at 1°	ARF FWHM at -4°	ARF FWHM at -6°	ARF FWHM at -7°
380 nm	1.17	1.15	1.25	1.24
800 nm	1.2	1.17	1.27	1.23
1600 nm	1.19	1.16	1.21	1.22
2500 nm	1.25	1.18	1.18	1.33

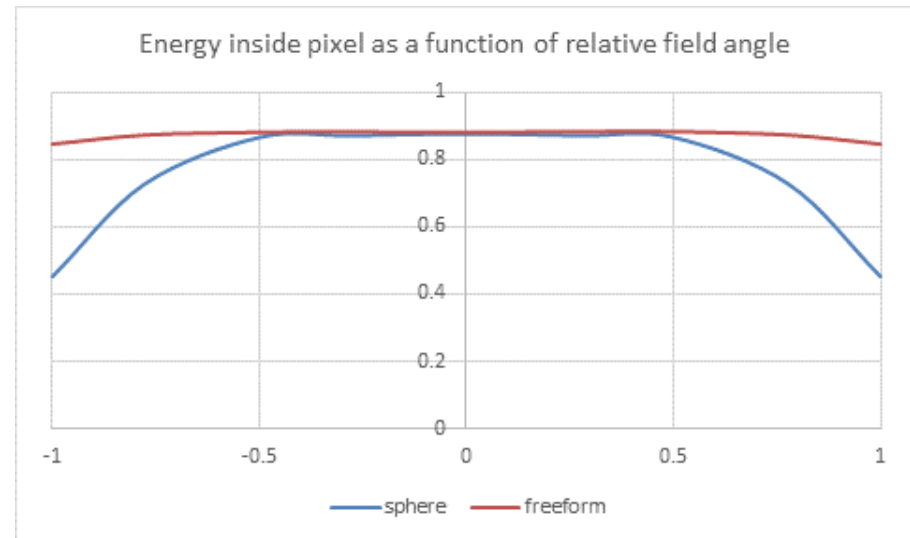
# Freeform optics examples



# High resolution, wide field Littrow-Offner for methane detection

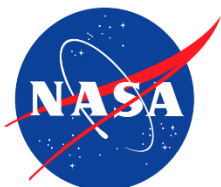


Parameter	Value
Spectral range (nm)	2,000-2,400
Spectral sampling (nm)	0.83
Detector pixel ( $\mu\text{m}$ )	30x30
Number of spatial pixels	1,240
F-number	4
Spot energy in pixel	>83% (>95% of diffraction limit)
Uniformity	>90%
Grating pitch ( $\mu\text{m}$ )	2.58
Size (optics)	90x90x190 mm

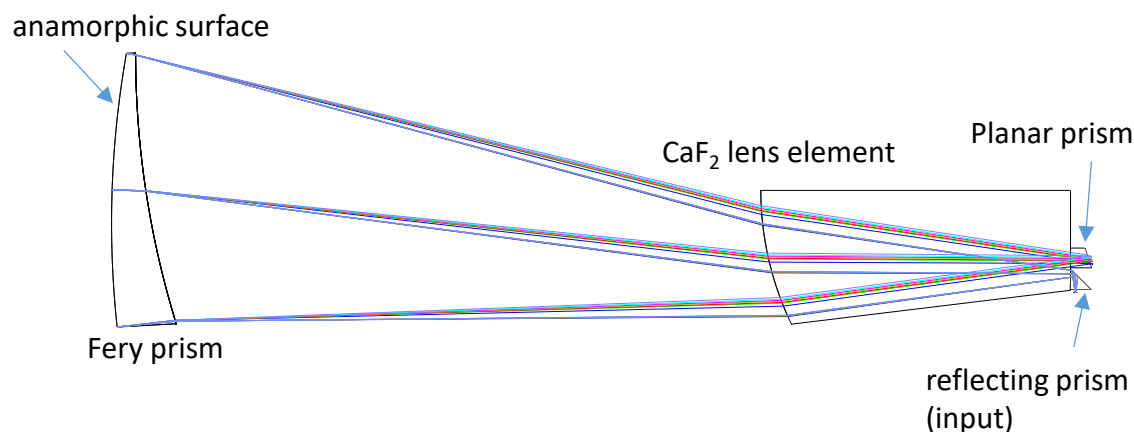


x-y polynomial surface with up to 14<sup>th</sup> order terms

Freeform surface doubles the field for the same spectrometer size



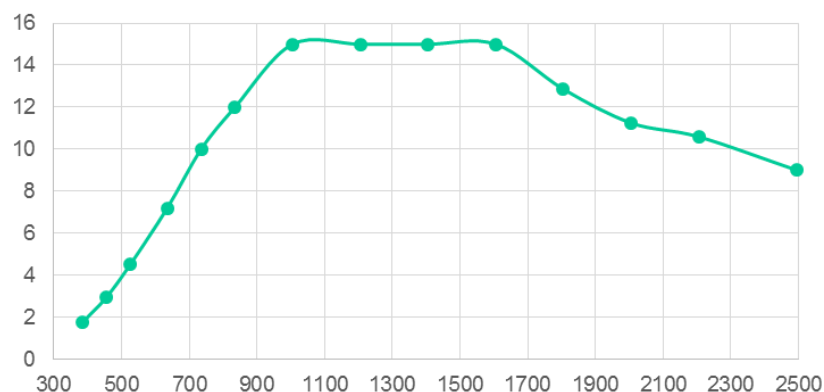
# Broadband refractive Dyson-type spectrometer with conventional surfaces

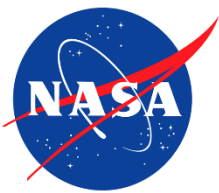


## Broad-band Prism Dyson Spectrometer (BPDS)

Spectral range	380 – 2500 nm single FPA
Spectral sampling	< 15 nm per pixel (variable)
Cross-track spatial elements	2160
Detector pixel size	18 $\mu\text{m}$
F-no	2.5
Uniformity	>90%
Dispersive element	Infrasil reflecting Fery prism with anamorphic surface
Optical design	Dyson with $\text{CaF}_2$ lens element

dispersion in nm per pixel as a function of wavelength



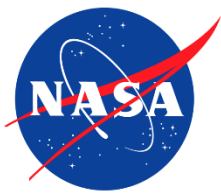


## Broadband Prism Dyson Spectrometer with freeform surface

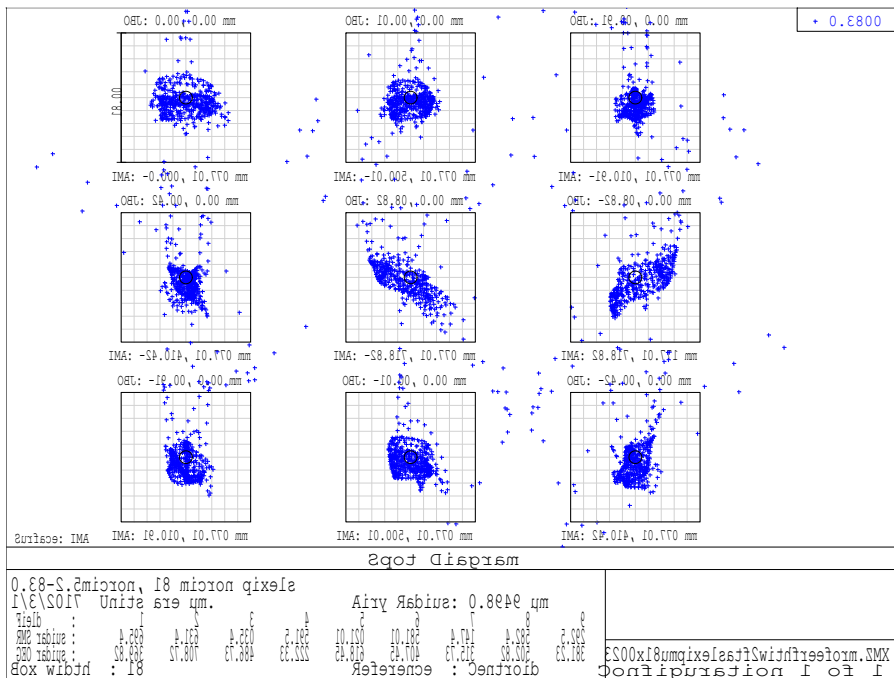
Broad-band Prism Dyson Spectrometer (BPDS)		BPDS with freeform surface	
Spectral range	380 – 2500 nm single FPA	Spectral range	380 – 2500 nm single FPA
Spectral sampling	< 15 nm per pixel (variable)	Spectral sampling	< 15 nm per pixel (variable)
Cross-track spatial elements	2160	Cross-track spatial elements	3200
Detector pixel size	18 $\mu\text{m}$	Detector pixel size	18 $\mu\text{m}$
F-no	2.5	F-no	2
Uniformity	>90%	Uniformity	>90%
Dispersive element	Infrasil reflecting Fery prism with anamorphic surface	Dispersive element	Infrasil reflecting Fery prism with anamorphic surface
Optical design	Dyson with $\text{CaF}_2$ lens element, spherical surface	Optical design	Dyson with $\text{CaF}_2$ lens element and freeform surface
Optics length	50 cm	Optics length	54 cm
Prism diameter	14 cm	Prism diameter	19.2 cm

For a modest increase in size, freeform surface allows simultaneous 1.5x increase in throughput and field while maintaining uniformity.

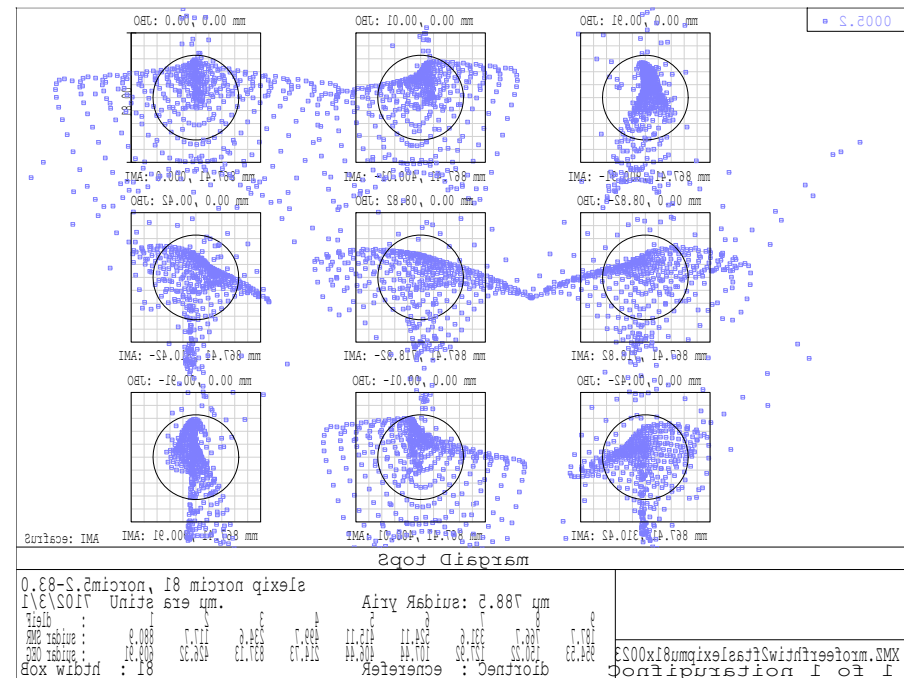




Spot sizes through field for 380 nm wavelength and 2500 nm wavelength, shown in 18  $\mu\text{m}$  pixel box size. The optimization accounts for wavefront rather than spot size, so it actually maximizes energy inside the pixel. See next chart.

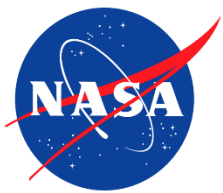


380 nm

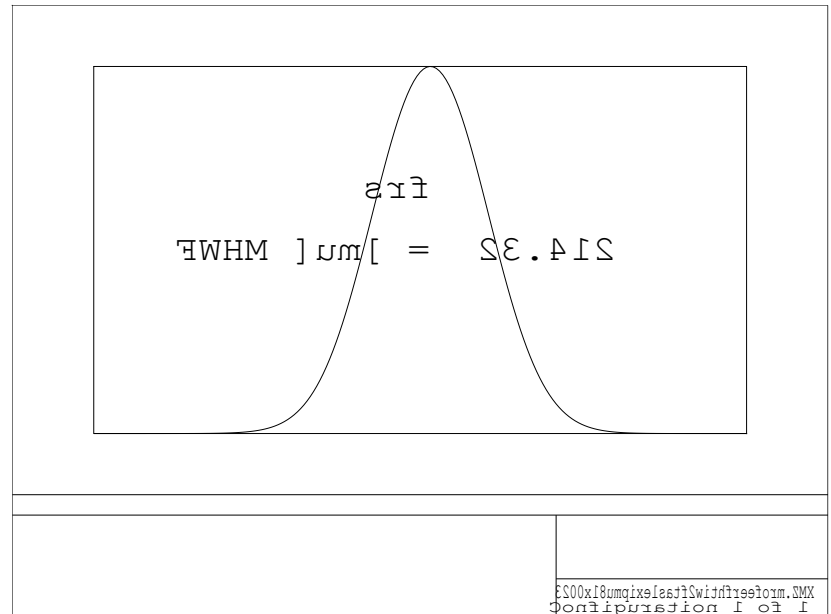
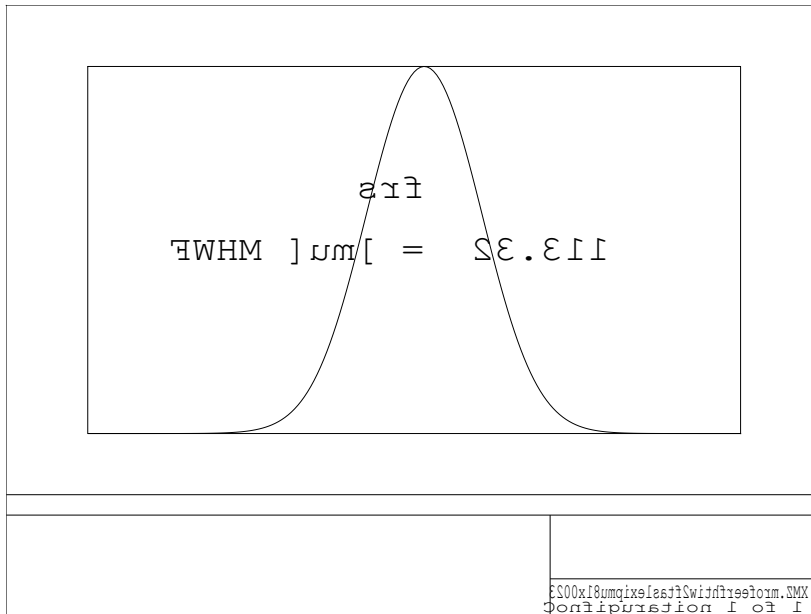


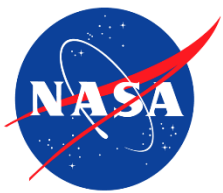
2500 nm



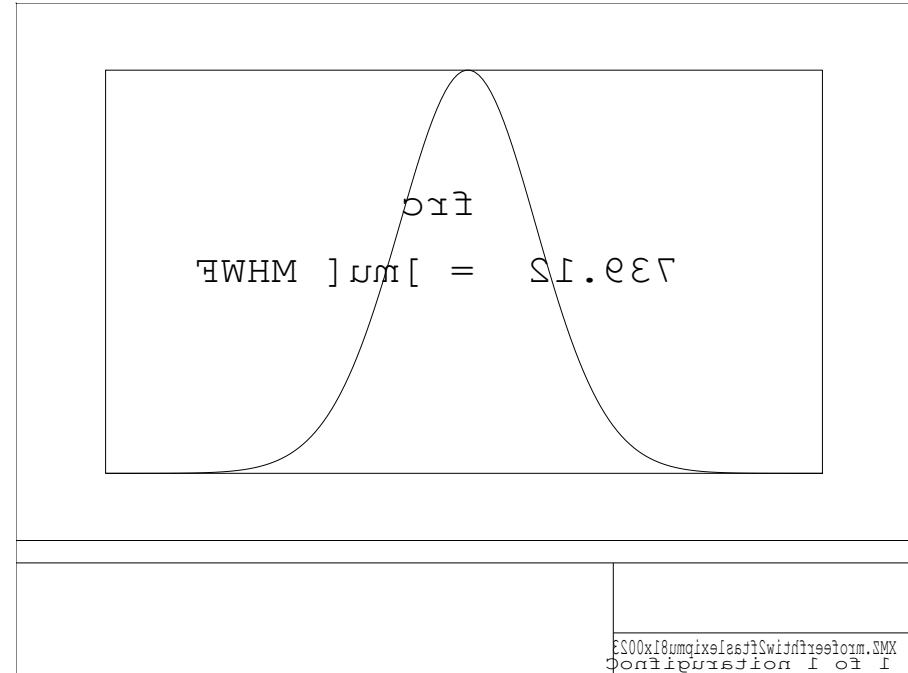
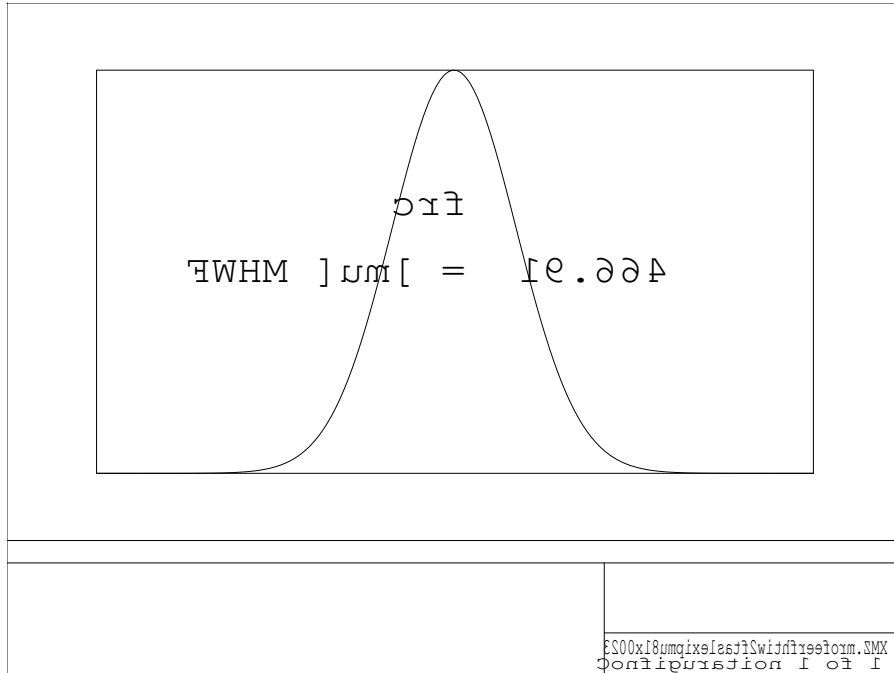


SRF variation through field is very small, example below for 1.2  $\mu\text{m}$ . Max smile is 0.6  $\mu\text{m}$  or 3.3%.

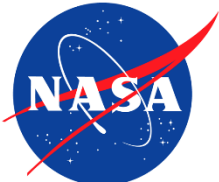




Maximum CRF FWHM variation through wavelength ~ 5.5%.  
Keystone is negligible < 0.2  $\mu\text{m}$ .



Contour plot of freeform surface with spherical term subtracted. Contour interval is 10  $\mu\text{m}$ .



# Conclusions

Utilizing the potential of imaging spectroscopy requires uncommon performance levels to be extracted from the instrument

Concentric imaging spectrometer forms have been advanced to very high levels of performance and are serving a wide range of applications

Design principles for telescope and spectrometer have been described and design/instrument examples based on these principles have been provided

Freeform optics can provide some theoretical advantages, remain to be proven in practice for these applications



## ACKNOWLEDGMENTS

Overall leadership in Imaging Spectroscopy: *Robert O. Green*

Grating development: *Daniel W. Wilson*

System/concept development: *Michael Eastwood, Byron Van Gorp*

Data reduction and algorithms: *David Thompson, Byron Van Gorp*

Component and subsystems: *Rich Muller, Victor White, Karl Yee, Holly Bender, Bill Johnson, Justin Haag, Lori Moore*

Detectors: *Teledyne*

Instrument teams: *Sarah Lundeen, Scott Nolte, Ian McCubbin, Justin Haag, Mark Helmlinger, Chuck Sarture, Bill Johnson*

Science Collaboration: *Diana Blaney, Heidi Dierssen, Bethany Ehlmann, Simon Hook, Joe Boardman, Michelle Gierach*